






## Lampiran 1. Data sheet Bejana Tekan 2nd Stage Compressor Suction KOD

Data Sheet for Unfired Pressure Vessels									
<b>Equipment Name:</b> 2nd Stage Compressor Suction KOD				<b>Location:</b> Arabian Gulf					
<b>Tag No.:</b> 603-11V-04				<b>Plant Location:</b> PS-3K					
<b>No. of Units:</b> 1				<b>Manufacturer/Model:</b>					
DESIGN DATA									
1	Orientation	Vertical		<b>CONSTRUCTION MATERIAL</b>					
2	Contents	HC, H <sub>2</sub> S, Water, CO <sub>2</sub>		Part	Material Specification				
3	Criticality Rating	3		Shell	SA537Cl.1 (note 4, 5, 6)				
4	Service	Lethal, Sour		Cladding/Lining of shell	See Note 4				
5	Design Code	ASME Sec. VIII DIV. 1		Heads	SA537Cl.1 (note 4, 5, 6)				
6	Code Stamp	Yes		Cladding/Lining of heads	See Note 4				
7				Supp. Skirt (Top/Bottom Section)	SA537Cl.1/SA283GR.C (note 9)				
8	Temperature			Self Reinforced Nozzles/Forged Flg. on CS	SA105				
9	Design - Upper/Lower	°C	150/-15	Self Reinforced Noz. above 3" on w eld dep	SA105 (note 4)				
10	Operating - Max./Normal / Min.	°C	45/35/35	Nozzle neck on w eld deposit	SB444Gr.1 UNS N06625				
11	Pressure			Forged Flanges above 3"NB on w eld depo	SA105 (note 4)				
12	Design (Internal)	barg	62 (note 10)	Forged Flanges 3"NB and below on w eld	SB564Gr.1 UNS N06625				
13	Design External	barg	Full Vacuum	Welding elbow	SB 366 UNS N06625				
14	Operating - Max/Norm/Min	barg	-/34/-	Demister	Solution Treated SS316L				
15	Corrosion Allowance	mm	3 mm on CS	Self Reinforcing Nozzles 3" NB	SB564Gr.1 UNS N06625				
16	Specific Gravity Liquid(HC/W)	Refer Sheet 2		and below on w eld deposit					
17	Gross Capacity	m <sup>3</sup>	10.4	Skirt Base ring/stiffeners	SA 283 GR C				
18	Vessel Dia (ID)	mm	1550	Nozzle neck on CS	SA106Gr.B -				
19	Vessel Length (T/L TO T/L)	mm	5000	Vortex Breakers	SB443 UNS N06625				
20	Shop Hydrotest Pressure (N&C)	Per code		Internal attachments on CS	SA 537Cl.1 -				
21	Wind	BS CP3, Chapter V, PART 2		Internal attachments on w eld deposit	Inconel 625				
22	Design Wind Speed	m/s	45	External attachments	SA 283 GR C				
23	Seismic	See note 9		External Bolts	SA 193 GR B7 (note 2)				
24	Shell Thickness (NOM)	mm	42/(39+3) mm w eld deposit (V)	Nuts	SA 194 GR 2H (note 2)				
25	Min. Head Thickness (Top/Bot)	mm	42/(38+3) mm w eld deposit (V)	Gaskets External	Spiral Wound (note 1)				
26	Skirt Thickness/Height	mm	8/1500 VTC	Gaskets Internal					
27	Weld Joint Efficiencies:			Internal Bolts	Solution Treated SS 316				
28	Shell	1.0		Nuts	Solution Treated SS 316				
29	Head	1.0							
30	Inspection and Testing			<b>CONSTRUCTION</b>					
31	Third Party Inspection	Yes		Type of Heads	2:1 Ellipsoidal				
32	Non Destructive Testing:			Type of support	Skirt				
33	Radiography	100%		Platform/Ladder/Pipe Clip	Required				
34	Ultrasonic	Yes, Per Code/Spec		Insulation supports	Not Required				
35	Magnetic Particle	100%		Manway Davit	Required				
36	Dye Penetrant	Per Code/Spec		Earthing Boss	Required				
37	Post Weld Heat Treatment	Yes		Lifting Lugs/Eyes/Trunions	Required				
38	Material Impact Test Required	Per code/spec		Name plate	Required, SS316				
39	Certified Elevated Temp. Test Required	No		<b>ESTIMATED WEIGHTS</b>					
40	Insulation (By others)	mm	No	Empty	Kg	14,500 VTC			
41	Fireproofing (By others)	mm	No	Shipping	Kg	VTA			
42	Painting (External)	ES-Q-12		Operating	Kg	20,400 VTC			
43	Painting (Internal)	No		Field Test	Kg	25,000 VTC			
44									
45				<b>NOTES:</b>					
46	1. Gaskets shall be SS316L spiral w ound graphite filled with SS316L internal and external rings. Gaskets shall be as per API-601.								
47	2. External bolting shall be hot dip galvanised as per BS 729 (BS EN ISO 1461:1999).								
48	3. Indicated thickness of shell, head and skirt are minimum and vendor to confirm the thicknesses.								
49	4. Inside surfaces of bottom half of the vessel upto 3200 mm height from bottom T/L, bottom head, nozzle sizes above 3" NB including								
50	gasket faces of flanges attached to the above section shall be w eld deposited with minimum 3 mm thick Inconel 625 before PWHT.								
51	5. Iron content in Inconel 625 w eld deposition shall not be more than 7%.								
52	6. Vessel shall meet all the requirements of NACE MR 0175 and the material shall be HIC tested as per NACE TM 0284.								
53	7. Material for shell and heads shall be of normalised steel, vacuum degassed and secondary calcium treated during manufacture. Max. carbon,								
54	sulphur content and CE shall not be more than 0.16%, 0.003% and 0.41% respectively.								
55	8. Nozzles shall be self reinforced (Integrally Reinforced) type w herever reinforcement is required.								
56	9. Inside diameter of 20"NB manway shall be 457 mm.								
57	10. Top 610 mm of skirt section w elded to bottom dished head shall be of the same material as bottom dished head.								
58	11. Refer Environmental data:1535-0-56-0001.								
59	12. Indicated design pressure is based on settle-out pressure and shall be confirmed during detail design.								
60	VTC: Vendor to confirm, VTA: Vendor to advise.								
1	30-Jul-01	APPROVED FOR DETAILED DESIGN		NVR	CPS	CPS	IDB		
0	24-06-2001	ISSUED FOR COMMENTS		NVR	GMP	CPS	IDB		
REV	DATE	ISSUE DESCRIPTION		ORIG	CHKD	APPRD.	PRJECT	CLIENT APPR.	
 <span style="font-size: 24px; font-weight: bold;">Worley</span>				 <span style="font-size: 18px; font-weight: bold;">Qatar Petroleum</span>				<b>Qatar Petroleum</b> <b>Bul Hanine Arab "C" Gas Cap Recycling</b>	
				Project No:		022/00705		Rev:	
				Document No:		00705-MEC-DTS-210		1	

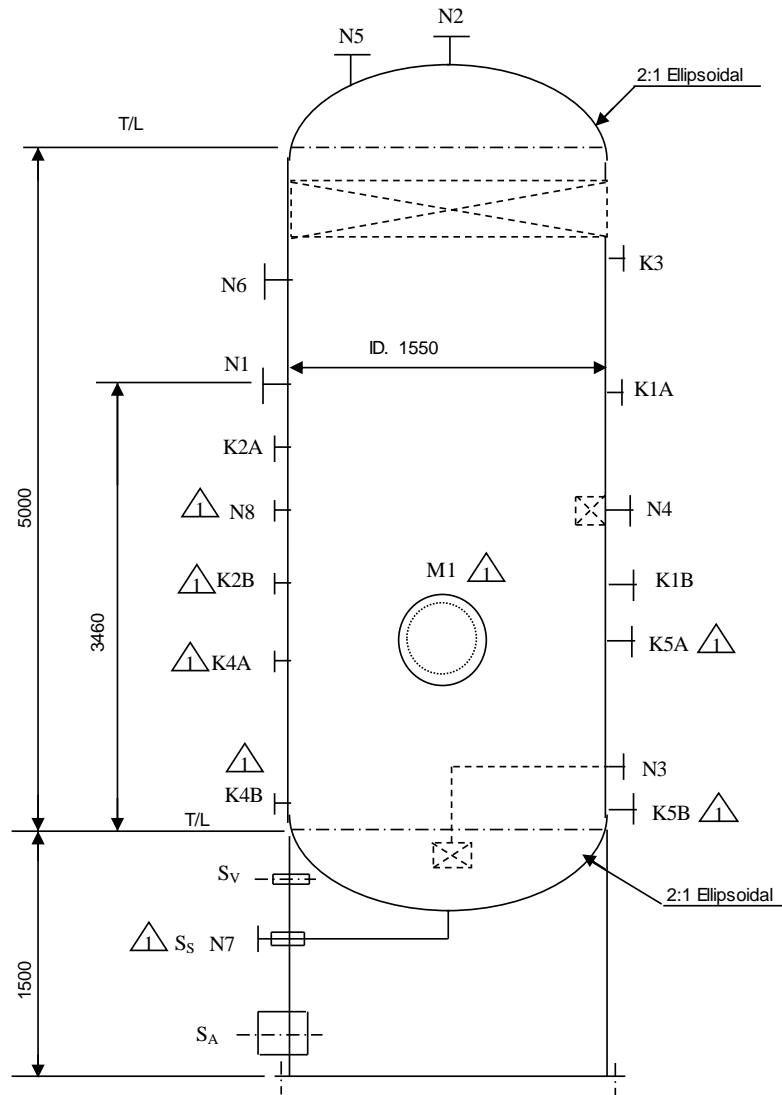
## Data Sheet for Unfired Pressure Vessel

<b>Equipment Name :</b> 2nd Stage Compressor Suction KOD		<b>Location:</b> Arabian Gulf							
<b>Tag No. :</b> 603-11V-04		<b>Plant Location :</b> PS-3K							
<b>No. of Units :</b> 1		<b>Manufacturer/Model :</b>							
<b>DESIGN DATA</b>									
1									
2	<b>Process Guarantees</b>								
3	Max liquid in Gas outlet shall not exceed 0.1 Usgal/MMSCF								
4	Max liquid particle size 20 micron in gas.								
5									
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<b>PROCESS DATA</b>									
12	Fluid Name	Wet Sour Gas							
13	Case	Rich Summer	Rich Winter	Lean Summer					
14	Vapour Flow rate	m3/h	1540	1653	884				
15	Vapour Density @ Oper. T/P	kg/m3	51	52	53				
16	Vapour Viscosity @ Oper. T/P	cP	0.013	0.013	0.013				
17	Vapour Molecular Weight		30	29	31				
18	Liquid HC Flow Rate	m3/h	9.8	12	38				
19	Liquid HC Density @ Oper. T/P	kg/m3	549	547	512				
20	Liquid HC Viscosity @ Oper. T/P	cP	0.12	0.12	0.1				
21	Liquid HC Surface Tension	dyne/cm	8.1	8.1	6.8				
22	Slug Holding Liquid Volume	m3/h	-	-	-				
23	Water Flow Rate	m3/h	0.04	0.04	0.01				
24	Water Density @ Oper. T/P	kg/m3	999	1000	992				
25	Water Viscosity @ Oper. T/P	cP	0.7	0.7	0.6				
26	Design Margin on Flow Rates	%	0	0	0				
27	Corrosive Compounds	H <sub>2</sub> S, CO <sub>2</sub> , Water							
28	<b>VESSEL INTERNALS</b>								
29	Gas Demister/Vane Pack	Mist Mat							
30	Vortex Breakers	N3 & N4							
<b>NOZZLE SCHEDULE</b>									
32	Mark No	Size	Qty.	Flange	Service	Standout (mm)		Reinf Pad (mm)	
33		NPS	Nos.	Rating Type/Face		Ext	Int	Thick	Diam
34	N1	16"	1	600# SR / RF	Fluid Inlet				
35	N2	10"	1	600# SR / RF	Vapour Outlet				
36	N3	2"	1	600# WN / RF	Water Outlet				
37	N4	6"	1	600# SR / RF	Hydrocarbon Outlet	△			
38	N5	2"	1	600# WN / RF	Vent				
39	N6	4"	1	600# SR / RF	PSV	△			
40	N7	3"	1	600# SR / RF	Drain				
41	N8	2"	1	600# WN / RF	Utility Connection	△			
42									
43	K1A/B	4"	2	600# SR / RF	Condensate Level Bridle				
44	K2A/B	4"	2	600# SR / RF	Condensate Level Bridle				
45	K3	2"	1	600# WN / RF	Pressure Transmitter				
46	K4A/B	4"	2	600# SR / RF	Water Level Bridle				
47	K5A/B	4"	2	600# SR / RF	Water Level Bridle				
48									
49	M1	20"	1	600# SR / RF	Manway				
50									
51	S <sub>A</sub>	ID.610	1	-	-	Skirt Access			
52	S <sub>v</sub>	2"	4	-	-	Skirt Vent			
53	S <sub>s</sub>	6"	1	-	-	Skirt Sleeve			
<b>REMARKS</b>									
55	1. Nozzle sizes and elevations shall be confirmed during detailed engineering.								
56	2. SR RF - Self Reinforced (Integrally Reinforced) nozzle with Raised Face Flange.								
57	3. Vendor to provide details of mist mat.								
 <b>Worley</b>						 <b>Qatar Petroleum</b>			
 <b>Qatar Petroleum</b>						<b>Qatar Petroleum</b> Bul Hanine Arab "C" Gas Cap Recycling Project No: 022/00705      Rev: 1 Document No: 00705-MEC-DTS-210			

## Data Sheet for Unfired Pressure Vessel

<b>Equipment Name :</b> 2nd Stage Compressor Suction KOD	<b>Location:</b> Arabian Gulf
<b>Tag No. :</b> 603-11V-04	<b>Plant Location :</b> PS-3K
<b>No. of Units :</b> 1	<b>Manufacturer/Model :</b>

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LIQUID LEVELS		HC LIQUID	WATER
53	LLHH mm	2850	750
54	LAH mm	2450	600
55	NLL mm	1970	450
56	LAL mm	1490	300
57	LALL mm	1170	150

Note: Vessel tan line = '0' Datum



Worley



**Qatar Petroleum**

**Bul Hanine Arab "C" Gas Cap Recycling**

<b>Project No:</b> 022/00705	<b>Rev:</b>
<b>Document No:</b> 00705-MEC-DTS-210	<b>1</b>

## Lampiran 2. ASME B3.13 untuk Material SA 537 Cl

STD-ASME B31.3-ENGL 1999 ■ 0759670 0607945 108 ■

Table A-1

ASME B31.3-1999 Edition

**TABLE A-1 (CONT'D)**  
**BASIC ALLOWABLE STRESSES IN TENSION FOR METALS<sup>1</sup>**  
 Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Material	Spec. No.	P-No. or S-No. (S)	Grade	Notes	Min. Temp., °F (6)	Specified Min. Strength, ksi		Min. Temp.			
						Tensile	Yield	to 100	200	300	
Carbon Steel (Cont'd)											
Pipes and Tubes (2) (Cont'd)											
...	A 53	1	B	(57)(59)	}	B	60	35	20.0	20.0	20.0
...	A 106	1	B	(57)							
...	A 333	1	6	(57)							
...	A 334										
...	A 369										
...	A 381	S-1	Y35	...	}	A	60	35	20.0	20.0	20.0
...	API 5L	S-1	B	(57)(59)(77)							
...	A 139	S-1	C	(86)	}	A	60	42	20.0	20.0	20.0
...	A 139	S-1	D	(86)							
...	API 5L	S-1	X42	(55)(77)	}	A	60	42	20.0	20.0	20.0
...	A 381	S-1	Y42	...							
...	A 381	S-1	Y48	...	}	A	62	48	20.6	19.7	18.7
...	API 5L	S-1	X46	(55)(77)							
...	A 381	S-1	Y46	...	}	A	63	46	21.0	21.0	21.0
...	A 381	S-1	Y50	...							
...	A 381	S-1	Y50	...	}	A	64	50	21.3	20.3	19.3
...	API 5L	S-1	X46	(55)(77)							
...	A 381	S-1	Y46	...	}	A	63	46	21.0	21.0	21.0
...	A 381	S-1	Y50	...							
A 516 Gr. 65	A 671	1	CC65	(57)(67)	}	B	65	35	21.7	21.3	20.7
A 515 Gr. 65	A 671	1	CB65	(57)(67)							
A 515 Gr. 65	A 672	1	B65	(57)(67)	}	A	65	35	21.7	21.3	20.7
A 516 Gr. 65	A 672	1	C65	(57)(67)							
...	A 139	S-1	E	(86)	}	A	66	52	22.0	22.0	22.0
...	API 5L	S-1	X52	(55)(77)							
...	A 381	S-1	Y52	...	}	A	66	52	22.0	22.0	22.0
...	A 381	S-1	Y52	...							
A 516 Gr. 70	A 671	1	CC70	(57)(67)	}	B	70	38	23.3	23.1	22.5
A 515 Gr. 70	A 671	1	CB70	(57)(67)							
A 515 Gr. 70	A 672	1	B70	(57)(67)	}	A	70	38	23.3	23.1	22.5
A 516 Gr. 70	A 672	1	C70	(57)(67)							
...	A 106	1	C	(57)	}	B	70	40	23.3	23.3	23.3
...	A 381	S-1	Y56	(51)(55)(71)(77)							
A 537 Cl. 1 (≤ 2½ in. thick)	A 671	1	CD70	}	(67)	D	70	50	23.3	23.3	22.9
A 537 Cl. 1 (≤ 2½ in. thick)	A 672	1	D70								
A 537 Cl. 1 (≤ 2½ in. thick)	A 691	1	CMSH70								
...	API 5L	S-1	X56	(51)(55)(71)(77)	}	A	71	56	23.7	23.7	23.7
...	A 381	S-1	Y56	(51)(55)(71)							

TABLE A-1 (CONT'D)  
BASIC ALLOWABLE STRESSES IN TENSION FOR METALS<sup>1</sup>

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Basic Allowable Stress S, ksi (1), at Metal Temperature, °F (7)													Grade	Spec. No.
400	500	600	650	700	750	800	850	900	950	1000	1050	1100	Carbon Steel (Cont'd) Pipes and Tubes (2) (Cont'd)	
20.0	18.9	17.3	17.0	16.5	13.0	10.8	8.7	6.5	4.5	2.5	1.6	1.0	B	A 53
													B	A 106
													A	A 333
													A	A 334
													FPB	A 369
													Y35	A 381
													B	API 5L
													C	A 139
													D	A 139
20.0	...	...	...	...	...	...	...	...	...	...	...	...	X42	API 5L
20.0	...	...	...	...	...	...	...	...	...	...	...	...	Y42	A 381
17.8	16.9	16.0	15.5	...	...	...	...	...	...	...	...	...	Y48	A 381
21.0	...	...	...	...	...	...	...	...	...	...	...	...	X46	API 5L
21.0	...	...	...	...	...	...	...	...	...	...	...	...	Y46	A 381
18.4	17.4	16.5	16.0	...	...	...	...	...	...	...	...	...	Y50	A 381
20.0	18.9	17.3	17.0	16.8	13.9	11.4	9.0	6.5	4.5	2.5	...	...	CC65	A 671
20.0	18.9	17.3	17.0	16.8	13.9	11.4	9.0	6.5	4.5	2.5	1.6	1.0	CB65	A 671
													B65	A 672
													C65	A 672
...	...	...	...	...	...	...	...	...	...	...	...	...	E	A 139
22.0	...	...	...	...	...	...	...	...	...	...	...	...	X52	API 5L
22.0	...	...	...	...	...	...	...	...	...	...	...	...	Y52	A 381
21.7	20.5	18.7	18.4	18.3	14.8	12.0	9.3	6.5	4.5	2.5	...	...	CC70	A 671
21.7	20.5	18.7	18.4	18.3	14.8	12.0	9.3	6.5	4.5	2.5	1.6	1.0	CB70	A 671
													B70	A 672
													C70	A 672
22.9	21.6	19.7	19.4	19.2	14.8	12.0	...	...	...	...	...	...	C	A 106
													CD70	A 671
22.9	22.9	22.6	22.0	21.4	...	...	...	...	...	...	...	...	D70	A 672
													CMSH70	A 691
23.7	...	...	...	...	...	...	...	...	...	...	...	...	X56	API 5L
23.7	...	...	...	...	...	...	...	...	...	...	...	...	Y56	A 381

### Lampiran 3. ASME B3.13 untuk Material SA 105

STD-ASME B31.3-ENGL 1999 ■ 0759670 0607951 401 ■

Table A-1

ASME B31.3-1999 Edition

**TABLE A-1 (CONT'D)**  
**BASIC ALLOWABLE STRESSES IN TENSION FOR METALS<sup>1</sup>**

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Material	Spec. No.	P-No. or S-No. (5)	Grade	Notes	Min. Temp., °F (6)	Specified Min. Strength, ksi		Min. Temp.		
						Tensile	Yield	to 100	200	300
<b>Carbon Steel (Cont'd)</b>										
<b>Forgings and Fittings (2)</b>										
...	A 350	1	LF-1	(9)(57)(59)	-20	60	30	20.0	18.3	17.7
...	A 181	1	CL 60	(9)(57)(59)	A	60	30	20.0	18.3	17.7
...	A 420	1	WPL-6	(57)	-50	60	35	20.0	20.0	20.0
...	A 234	1	WPB	(57)(59)	B	60	35	20.0	20.0	20.0
...	A 350	1	LF-2	(9)(57)	-50	70	36	23.3	21.9	21.3
...	A 105	1	...	(9)(57)(59)	-20	70	36	23.3	21.9	21.3
...	A 181	1	CL 70	(9)(57)(59)	A					
...	A 234	1	WPC	(57)(59)	B	70	40	23.3	23.3	23.3
<b>Castings (2)</b>										
...	A 216	1	WCA	(57)	-20	60	30	20.0	18.3	17.7
...	A 352	1	LCB	(9)(57)	-50	65	35	21.7	21.3	20.7
...	A 216	1	WCB	(9)(57)	-20	70	36	23.3	21.9	21.3
...	A 216	1	WCC	(9)(57)	-20	70	40	23.3	23.3	23.3

ASME B31.3-1999 Edition

Table A-1

TABLE A-1 (CONT'D)  
BASIC ALLOWABLE STRESSES IN TENSION FOR METALS<sup>1</sup>

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Basic Allowable Stress $S$ , ksi (1), at Metal Temperature, °F (7)														Grade	Spec. No.
400	500	600	650	700	750	800	850	900	950	1000	1050	1100			
														Carbon Steel (Cont'd) Forgings and Fittings (2)	
17.2	16.2	14.8	14.5	14.4	13.0	10.8	7.8	5.0	3.0	1.5	...	...	LF-1	A 350	
17.2	16.2	14.8	14.5	14.4	13.0	10.8	8.7	6.5	4.5	2.5	1.6	1.0	CL 60	A 181	
20.0	18.9	17.3	17.0	16.8	13.0	10.8	7.8	5.0	3.0	1.5	...	...	WPL-4	A 420	
20.0	18.9	17.3	17.0	16.8	13.0	10.8	8.7	6.5	4.5	2.5	1.6	1.0	WPB	A 234	
20.6	19.4	17.8	17.4	17.3	14.8	12.0	7.8	5.0	3.0	1.5	...	...	LF-2	A 350	
20.6	19.4	17.8	17.4	17.3	14.8	12.0	9.3	6.5	4.5	2.5	1.6	1.0	...	A 105	
													CL 70	A 181	
22.9	21.6	19.7	19.4	19.2	14.8	12.0	...	...	...	...	...	...	WPC	A 234	
														Castings (2)	
17.2	16.2	14.8	14.5	14.4	13.0	10.8	8.6	6.5	4.5	2.5	1.6	1.0	WCA	A 216	
20.0	18.9	17.3	17.0	16.8	13.0	11.4	8.9	6.5	4.5	2.5	1.6	1.0	LCB	A 352	
20.6	19.4	17.8	17.4	17.3	14.8	12.0	9.3	6.5	4.5	2.5	1.6	1.0	WCB	A 216	
22.9	21.6	19.7	19.4	19.2	14.8	12.0	9.3	6.5	4.5	2.5	...	...	WCC	A 216	

## Lampiran 4. ASME B16.5 untuk material SA 105

PIPE FLANGES AND FLANGED FITTINGS

ASME B16.5-1996

**TABLES 2**  
**PRESSURE-TEMPERATURE RATINGS FOR**  
**GROUPS 1.1 THROUGH 3.16 MATERIALS**

**TABLE 2-1.1 RATINGS FOR GROUP 1.1 MATERIALS**

Nominal Designation	Forgings	Castings	Plates
C-Si	A 105 (1)	A 216 Gr. WCB (1)	A 516 Gr. 70 (1)
C-Mn-Si	A 350 Gr. LF2 (1)		A 516 Gr. 70 (1)(2) A 537 Cl. 1 (3)

**NOTES:**

(1) Upon prolonged exposure to temperatures above 800°F, the carbide phase of steel may be converted to graphite. Permissible, but not recommended for prolonged use above 800°F.

(2) Not to be used over 850°F.

(3) Not to be used over 700°F.

**WORKING PRESSURES BY CLASSES, psig**

Class Temp., °F	150	300	400	600	900	1500	2500
-20 to 100	285	740	990	1480	2220	3705	6170
200	260	675	900	1350	2025	3375	5625
300	230	655	875	1315	1970	3280	5470
400	200	635	845	1270	1900	3170	5280
500	170	600	800	1200	1795	2995	4990
600	140	550	730	1095	1640	2735	4560
650	125	535	715	1075	1610	2685	4475
700	110	535	710	1065	1600	2665	4440
750	95	505	670	1010	1510	2520	4200
800	80	410	550	825	1235	2060	3430
850	65	270	355	535	805	1340	2230
900	50	170	230	345	515	860	1430
950	35	105	140	205	310	515	860
1000	20	50	70	105	155	260	430



## Lampiran 5. ASME B16.5 untuk Material SB 564 Gr.1 UNS No 6625

ASME B16.5-1996

PIPE FLANGES AND FLANGED FITTINGS

**TABLE 2-3.8 RATINGS FOR GROUP 3.8 MATERIALS**

Nominal Designation	Forgings	Castings	Plates
54Ni-16Mo-15Cr	B 564 Gr. N10276 (1)(4)		B 575 Gr. N10276 (1)(4)
60Ni-22Cr-9Mo-3.5Cb	B 564 Gr. N06625 (3)(5)		B 443 Gr. N06625 (3)(5)
62Ni-28Mo-5Fe	B 335 Gr. N10001 (1)(2)(6)		B 333 Gr. N10001 (1)(6)
70Ni-16Mo-7Cr-5Fe	B 573 Gr. N10003 (2)(3)		B 434 Gr. N10003 (3)
61Ni-16Mo-16Cr	B 574 Gr. N06455 (1)(2)(6)		B 575 Gr. N06455 (1)(6)
42Ni-21.5Fe-3Cr-2.3Cu	B 564 Gr. N08825 (3)(7)		B 424 Gr. N08825 (3)(7)

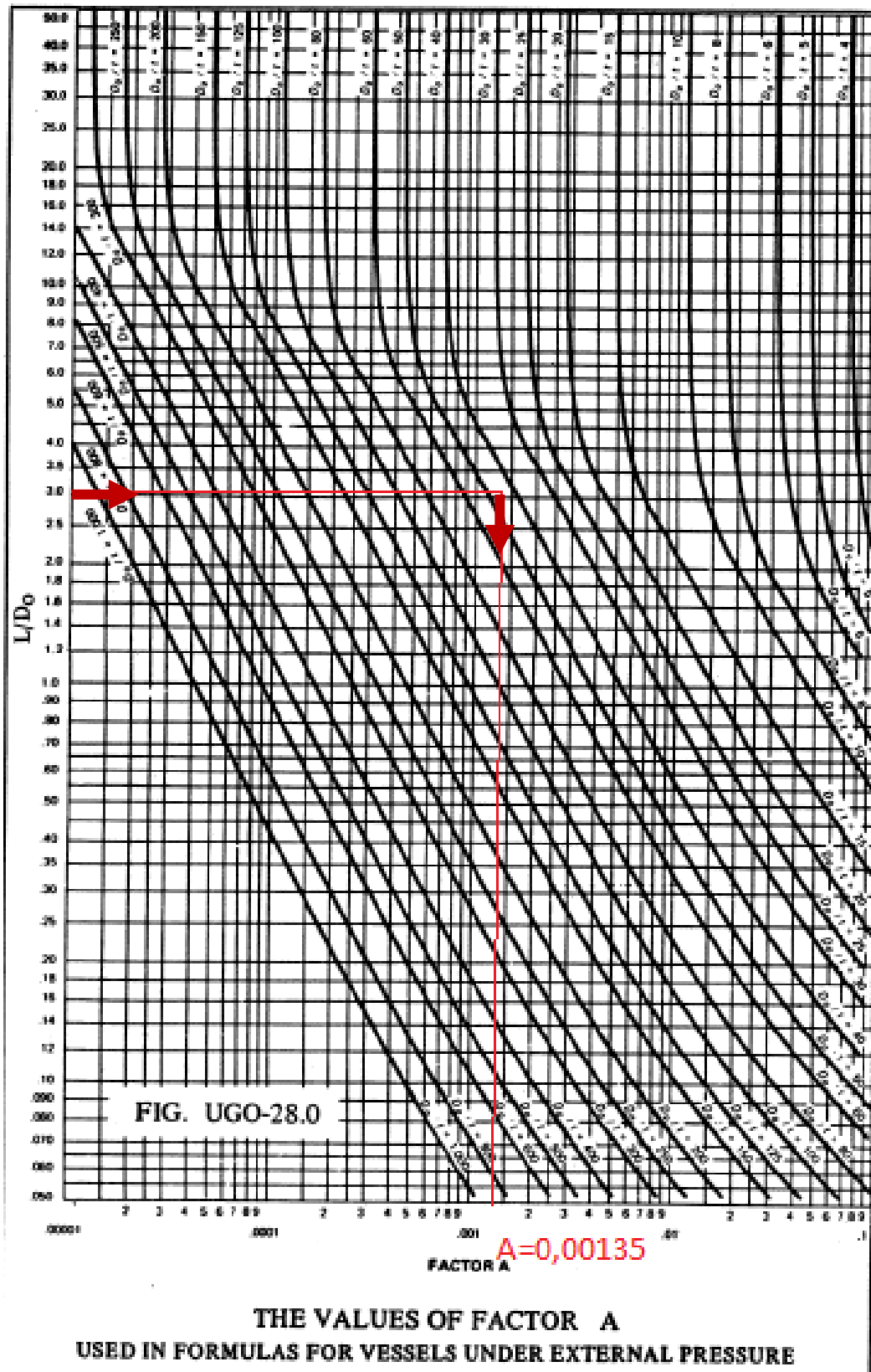
**NOTES:**

- (1) Use solution annealed material only.
- (2) The chemical composition, mechanical properties, heat treating requirements, and grain size requirements shall conform to the applicable ASTM specification. The manufacturing procedures, tolerances, tests, certification, and markings shall be in accordance with ASTM B 564.
- (3) Use annealed material only.
- (4) Not to be used over 1250°F.
- (5) Not to be used over 1200°F. Alloy N06625 in the annealed condition is subject to severe loss of impact strength at room temperatures after exposure in the range of 1000°F to 1400°F.
- (6) Not to be used over 800°F.
- (7) Not to be used over 1000°F.

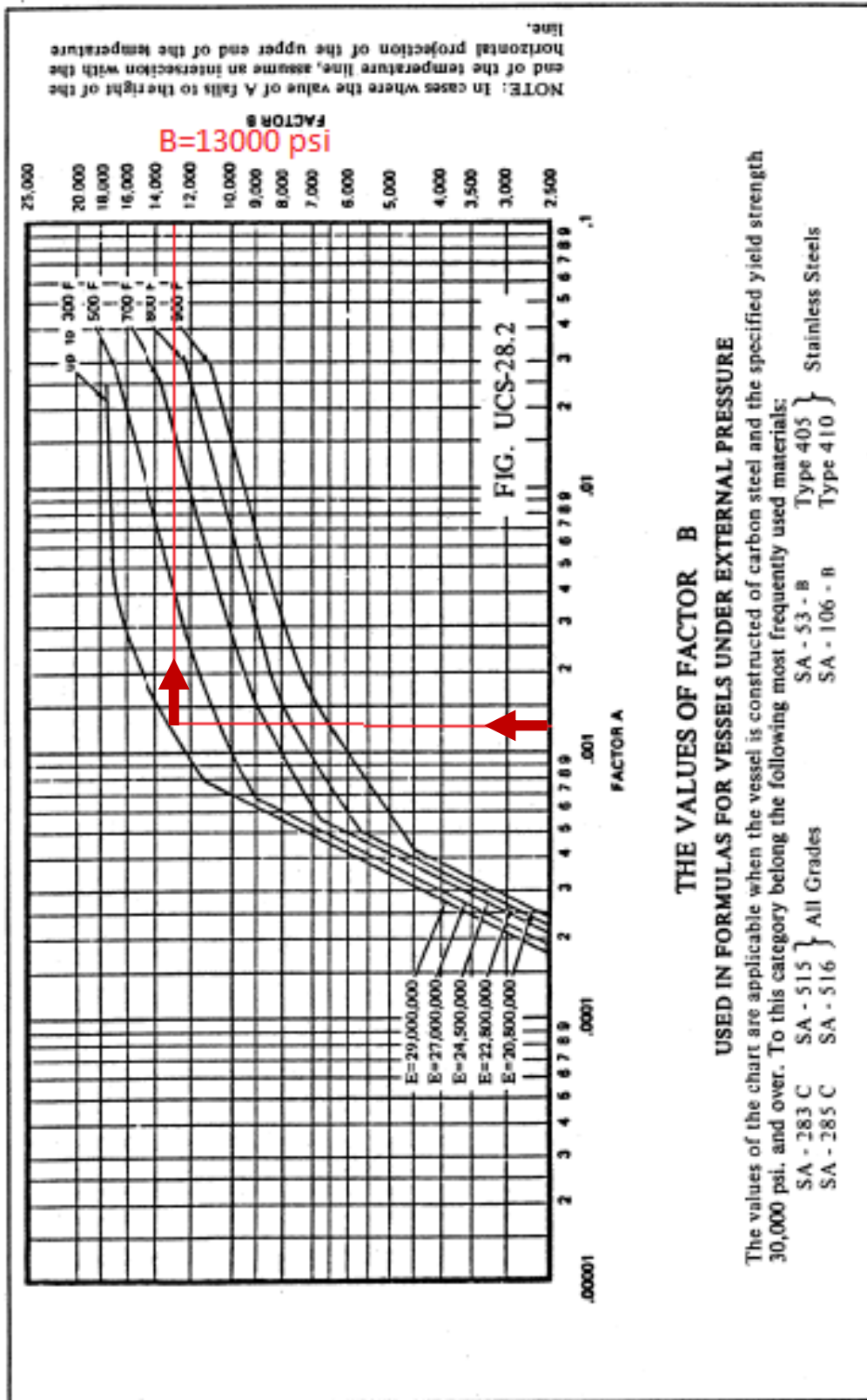
**WORKING PRESSURES BY CLASSES, psig**

Class Temp., °F	150	300	400	600	900	1500	2500
-20 to 100	290	750	1000	1500	2250	3750	6250
200	260	750	1000	1500	2250	3750	6250
300	230	730	970	1455	2185	3640	6070
400	200	705	940	1410	2115	3530	5880
500	170	665	885	1330	1995	3325	5540
600	140	605	805	1210	1815	3025	5040
650	125	590	785	1175	1765	2940	4905
700	110	570	755	1135	1705	2840	4730
750	95	530	710	1065	1595	2660	4430
800	80	510	675	1015	1525	2540	4230
850	65	485	650	975	1460	2435	4060
900	50	450	600	900	1350	2245	3745
950	35	385	515	775	1160	1930	3220
1000	20	365	485	725	1090	1820	3030
1050	...	360	480	720	1080	1800	3000
1100	...	325	430	645	965	1610	2685
1150	...	275	365	550	825	1370	2285
1200	...	185	245	370	555	925	1545
1250	...	145	195	295	440	735	1220
1300	...	110	145	215	325	540	900

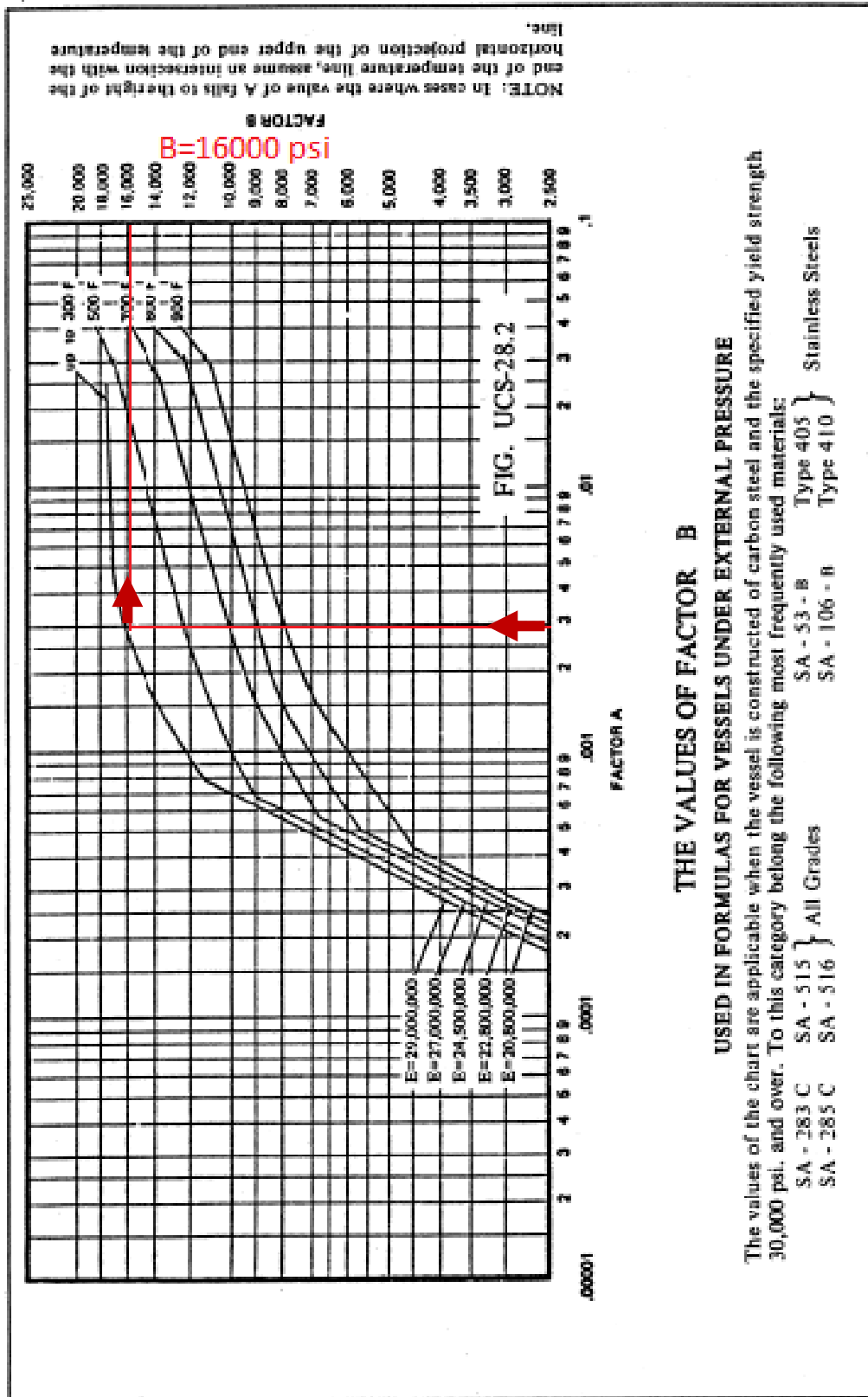
Lampiran 6. Nilai Faktor A untuk Shell



Lampiran 7. Nilai B untuk Shell



## Lampiran 8. Nilai B untuk Head

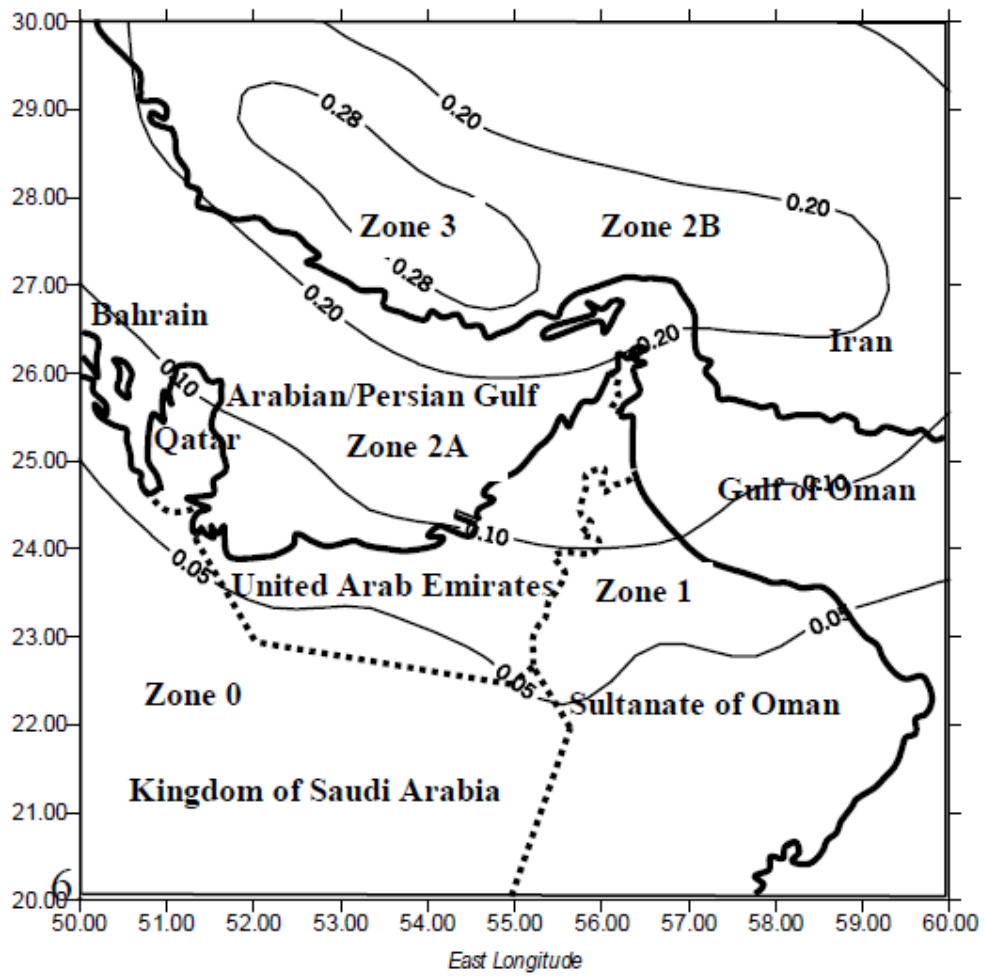


## Lampiran 9. Ukuran Tebal Dinding Standar

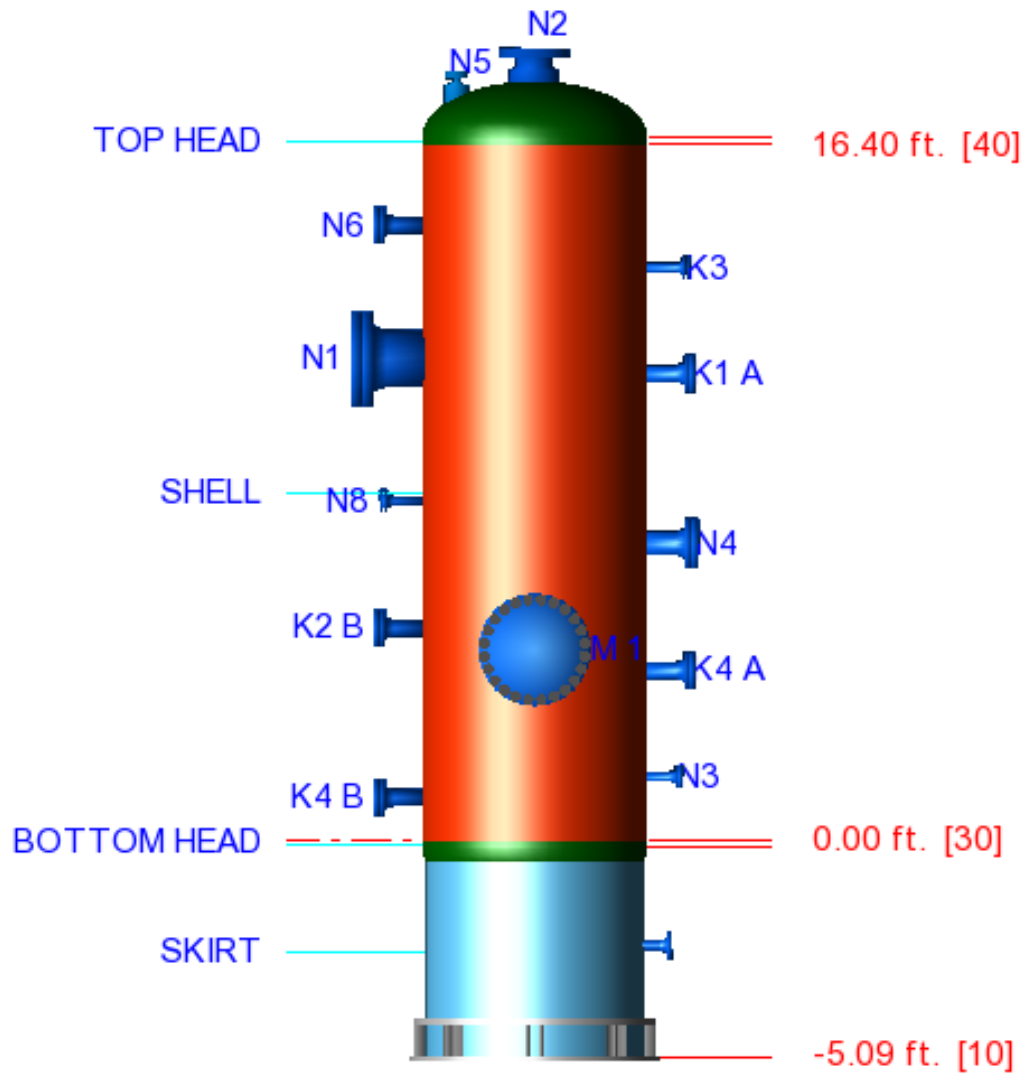
### Ukuran Tebal Dinding Shell & Head Standar (in):

- 1/4 = 0,25	- 7/8 = 0,875	- 1-1/2 = 1,5
- 5/16 = 0,3125	- 15/16 = 0,9375	- 1-9/16 = 1,5625
- 3/8 = 0,375	- 1 = 1,0	- 1-5/8 = 1,625
- 7/16 = 0,4375	- 1-1/16 = 1,0625	- 1-11/16 = 0,6875
- 1/2 = 0,5	- 1-1/8 = 1,125	- 1-3/4 = 1,75
- 9/16 = 0,5625	- 1-3/16 = 1,1875	- 1-13/16 = 1,8125
- 5/8 = 0,625	- 1-1/4 = 1,25	- 1-7/8 = 1,875
- 11/16 = 0,6875	- 1-5/16 = 1,3125	- 1-15/16 = 1,9375
- 3/4 = 0,75	- 1-3/8 = 1,375	- 2 = 2,0
- 13/16 = 0,8125	- 1-7/16 = 1,4375	- 2-1/4 = 2,25

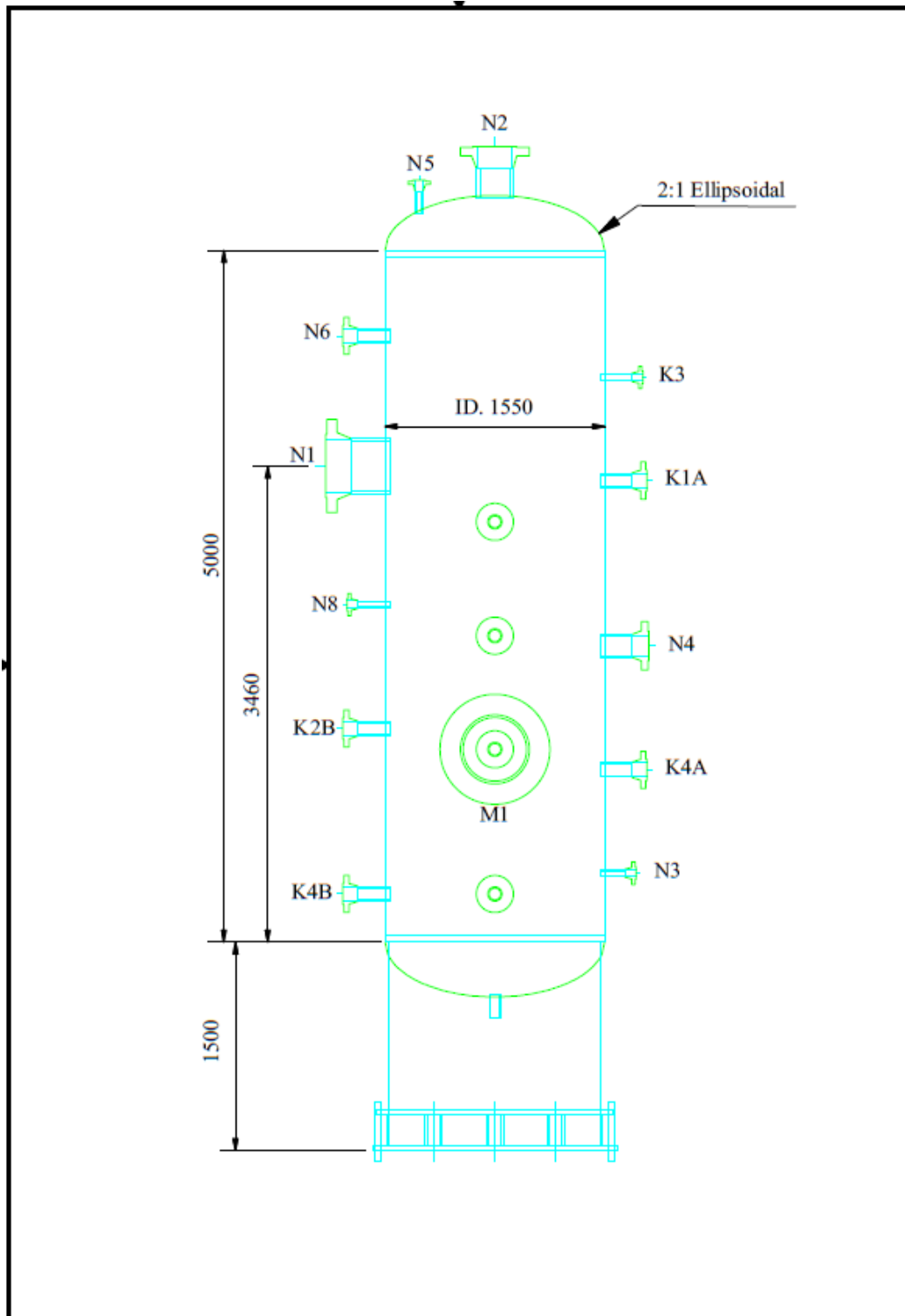
Lampiran 10. *Seismic Zone Map UAE*



Lampiran 11. Gambar Hasil Perancangan *Software PV Elite 2014*



Lampiran 12. Gambar Hasil Perancangan





### Lampiran 13. Analisa PV Elite *Element Thickness*

#### **Element Thickness, Pressure, Diameter and Allowable Stress :**

		Int. Press	Nominal	Total Corr	Element	Allowable
From	To	+ Liq. Hd	Thickness	Allowance	Diameter	
Stress (SE)		psig	in.	in.	in.	psi

SKIRT	...		0.31496	0.11811	61.0235	
BOTTOM HEA	22900.0	903.139	1.37500	0.11811	61.0235	
SHELL	22900.0	903.139	1.37500	0.11811	61.0235	
TOP HEAD	22594.0	899.235	1.37500	0.11811	61.0235	

#### **Element Required Thickness and MAWP :**

Required		Design	M.A.W.P.	M.A.P.	Minimum	
From	To	Pressure	Corroded	New & Cold	Thickness	
Thickness		psig	psig	psig	in.	

SKIRT	...		No Calc	No Calc	0.31496	No
BOTTOM HEA	1.32469	899.235	913.212	1027.35	1.37500	
SHELL	1.35538	899.235	913.212	1004.81	1.37500	
TOP HEAD	1.33578	899.235	904.862	1027.35	1.37500	
Minimum			904.862	1004.810		

## Lampiran 14. Analisa PV Elite *Internal Pressure*

### Internal Pressure Calculation Results :

**ASME Code, Section VIII, Division 1, 2013**

**Elliptical Head From 20 To 30 SA-537 , UCS-66 Crv. D at 302 °F**

**BOTTOM HEAD**

Longitudinal Joint: Full Radiography per UW-11(a) Type 1  
Circumferential Joint: Full Radiography per UW-11(a) Type 1

Material UNS Number: K12437

Required Thickness due to Internal Pressure [tr]:

$$\begin{aligned} &= (P \cdot D \cdot K_{cor}) / (2 \cdot S \cdot E - 0.2 \cdot P) \text{ Appendix 1-4 (c)} \\ &= (903.139 \cdot 61.2597 \cdot 0.995) / (2 \cdot 22900.00 \cdot 1.00 - 0.2 \cdot 903.139) \\ &= 1.2066 + 0.1181 = 1.3247 \text{ in.} \end{aligned}$$

Max. Allowable Working Pressure at given Thickness, corroded [MAWP]:

**Less Operating Hydrostatic Head Pressure of 3.904 psig**

$$\begin{aligned} &= (2 \cdot S \cdot E \cdot t) / (K_{cor} \cdot D + 0.2 \cdot t) \text{ per Appendix 1-4 (c)} \\ &= (2 \cdot 22900.00 \cdot 1.00 \cdot 1.2569) / (0.995 \cdot 61.2597 + 0.2 \cdot 1.2569) \\ &= 940.645 - 3.904 = 936.741 \text{ psig} \end{aligned}$$

Maximum Allowable Pressure, New and Cold [MAPNC]:

$$\begin{aligned} &= (2 \cdot S \cdot E \cdot t) / (K \cdot D + 0.2 \cdot t) \text{ per Appendix 1-4 (c)} \\ &= (2 \cdot 22900.00 \cdot 1.00 \cdot 1.3750) / (1.000 \cdot 61.0235 + 0.2 \cdot 1.3750) \\ &= 1027.350 \text{ psig} \end{aligned}$$

Actual stress at given pressure and thickness, corroded [Sact]:

$$\begin{aligned} &= (P \cdot (K_{cor} \cdot D + 0.2 \cdot t)) / (2 \cdot E \cdot t) \\ &= (903.139 \cdot (0.995 \cdot 61.2597 + 0.2 \cdot 1.2569)) / (2 \cdot 1.00 \cdot 1.2569) \\ &= 21986.916 \text{ psi} \end{aligned}$$

Straight Flange Required Thickness:

$$\begin{aligned} &= (P \cdot R) / (S \cdot E - 0.6 \cdot P) + c \text{ per UG-27 (c) (1)} \\ &= (903.139 \cdot 30.6299) / (22900.00 \cdot 1.00 - 0.6 \cdot 903.139) + 0.118 \\ &= 1.355 \text{ in.} \end{aligned}$$

Straight Flange Maximum Allowable Working Pressure:

**Less Operating Hydrostatic Head Pressure of 3.904 psig**

$$\begin{aligned} &= (S \cdot E \cdot t) / (R + 0.6 \cdot t) \text{ per UG-27 (c) (1)} \\ &= (22900.00 \cdot 1.00 \cdot 1.2569) / (30.6299 + 0.6 \cdot 1.2569) \\ &= 917.117 - 3.904 = 913.212 \text{ psig} \end{aligned}$$

Factor K, corroded condition [Kcor]:

$$\begin{aligned} &= ( 2 + ( \text{Inside Diameter} / ( 2 \cdot \text{Inside Head Depth} ) )^2 ) / 6 \\ &= ( 2 + ( 61.260 / ( 2 \cdot 15.374 ) )^2 ) / 6 \\ &= 0.994888 \end{aligned}$$

Percent Elong. per UCS-79, VIII-1-01-57  $(75 \cdot t_{nom} / R_f) \cdot (1 - R_f / R_o)$  9.323 %

**Note: Please Check Requirements of UCS-79 as Elongation is > 5%.**

**MDMT Calculations in the Knuckle Portion:**

Govrn. thk, tg = 1.375 , tr = 1.214 , c = 0.1181 in. , E\* = 1.00  
Stress Ratio = tr \* (E\*)/(tg - c) = 0.966 , Temp. Reduction = 3 °F

Min Metal Temp. w/o impact per UCS-66, Curve D -17 °F  
Min Metal Temp. at Required thickness (UCS 66.1) -20 °F

**MDMT Calculations in the Head Straight Flange:**

Govrn. thk, tg = 1.375 , tr = 1.245 , c = 0.1181 in. , E\* = 1.00  
Stress Ratio = tr \* (E\*)/(tg - c) = 0.991 , Temp. Reduction = 1 °F

Min Metal Temp. w/o impact per UCS-66, Curve D -17 °F  
Min Metal Temp. at Required thickness (UCS 66.1) -18 °F

Note: Post Weld Heat Treatment is required for this Element/Joint.

**Cylindrical Shell From 30 To 40 SA-537 , UCS-66 Crv. D at 302 °F**

**SHELL**

Longitudinal Joint: Full Radiography per UW-11(a) Type 1  
Circumferential Joint: Full Radiography per UW-11(a) Type 1

Material UNS Number: K12437

Required Thickness due to Internal Pressure [tr]:  
= (P\*R)/(S\*E-0.6\*P) per UG-27 (c) (1)  
= (903.139\*30.6299)/(22900.00\*1.00-0.6\*903.139)  
= 1.2373 + 0.1181 = 1.3554 in.

Max. Allowable Working Pressure at given Thickness, corroded [MAWP]:  
Less Operating Hydrostatic Head Pressure of 3.904 psig  
= (S\*E\*t)/(R+0.6\*t) per UG-27 (c) (1)  
= (22900.00\*1.00\*1.2569)/(30.6299+0.6\*1.2569)  
= 917.117 - 3.904 = 913.212 psig

Maximum Allowable Pressure, New and Cold [MAPNC]:  
= (S\*E\*t)/(R+0.6\*t) per UG-27 (c) (1)  
= (22900.00\*1.00\*1.3750)/(30.5117+0.6\*1.3750)  
= 1004.811 psig

Actual stress at given pressure and thickness, corroded [Sact]:  
= (P\*(R+0.6\*t))/(E\*t)  
= (903.139\*(30.6299+0.6\*1.2569))/(1.00\*1.2569)  
= 22550.992 psi

Percent Elongation per UCS-79 (50\*t<sub>nom</sub>/R<sub>f</sub>)\*(1-R<sub>f</sub>/R<sub>o</sub>) 2.204 %

**Minimum Design Metal Temperature Results:**

Govrn. thk, tg = 1.375 , tr = 1.245 , c = 0.1181 in. , E\* = 1.00

Stress Ratio =  $tr * (E^*) / (tg - c) = 0.991$  , Temp. Reduction = 1 °F

Min Metal Temp. w/o impact per UCS-66, Curve D -17 °F  
Min Metal Temp. at Required thickness (UCS 66.1) -18 °F

Note: Post Weld Heat Treatment is required for this Element/Joint.

**Elliptical Head From 40 To 50 SA-537 , UCS-66 Crv. D at 302 °F**

TOP HEAD

Longitudinal Joint: Full Radiography per UW-11(a) Type 1  
Circumferential Joint: Full Radiography per UW-11(a) Type 1

Material UNS Number: K12437

Required Thickness due to Internal Pressure [tr]:

$$\begin{aligned} &= (P * D * K_{cor}) / (2 * S * E - 0.2 * P) \text{ Appendix 1-4 (c)} \\ &= (899.235 * 61.2597 * 0.995) / (2 * 22594.00 * 1.00 - 0.2 * 899.235) \\ &= 1.2177 + 0.1181 = 1.3358 \text{ in.} \end{aligned}$$

Max. Allowable Working Pressure at given Thickness, corroded [MAWP]:

$$\begin{aligned} &= (2 * S * E * t) / (K_{cor} * D + 0.2 * t) \text{ per Appendix 1-4 (c)} \\ &= (2 * 22594.00 * 1.00 * 1.2569) / (0.995 * 61.2597 + 0.2 * 1.2569) \\ &= 928.076 \text{ psig} \end{aligned}$$

Maximum Allowable Pressure, New and Cold [MAPNC]:

$$\begin{aligned} &= (2 * S * E * t) / (K * D + 0.2 * t) \text{ per Appendix 1-4 (c)} \\ &= (2 * 22900.00 * 1.00 * 1.3750) / (1.000 * 61.0235 + 0.2 * 1.3750) \\ &= 1027.350 \text{ psig} \end{aligned}$$

Actual stress at given pressure and thickness, corroded [Sact]:

$$\begin{aligned} &= (P * (K_{cor} * D + 0.2 * t)) / (2 * E * t) \\ &= (899.235 * (0.995 * 61.2597 + 0.2 * 1.2569)) / (2 * 1.00 * 1.2569) \\ &= 21891.867 \text{ psi} \end{aligned}$$

Straight Flange Required Thickness:

$$\begin{aligned} &= (P * R) / (S * E - 0.6 * P) + c \text{ per UG-27 (c) (1)} \\ &= (899.235 * 30.6299) / (22594.00 * 1.00 - 0.6 * 899.235) + 0.118 \\ &= 1.367 \text{ in.} \end{aligned}$$

Straight Flange Maximum Allowable Working Pressure:

$$\begin{aligned} &= (S * E * t) / (R + 0.6 * t) \text{ per UG-27 (c) (1)} \\ &= (22594.00 * 1.00 * 1.2569) / (30.6299 + 0.6 * 1.2569) \\ &= 904.862 \text{ psig} \end{aligned}$$

Factor K, corroded condition [Kcor]:

$$\begin{aligned} &= ( 2 + ( \text{Inside Diameter} / ( 2 * \text{Inside Head Depth} ) ) ^ (2) ) / 6 \\ &= ( 2 + ( 61.260 / ( 2 * 15.374 ) ) ^ (2) ) / 6 \\ &= 0.994888 \end{aligned}$$

Percent Elong. per UCS-79, VIII-1-01-57  $(75 * t_{nom} / R_f) * (1 - R_f / R_o) = 9.323 \%$

Note: Please Check Requirements of UCS-79 as Elongation is > 5%.

**MDMT Calculations in the Knuckle Portion:**

Govern. thk,  $t_g = 1.375$  ,  $t_r = 1.209$  ,  $c = 0.1181$  in. ,  $E^* = 1.00$   
Stress Ratio =  $t_r * (E^*) / (t_g - c) = 0.962$  , Temp. Reduction = 4 °F

Min Metal Temp. w/o impact per UCS-66, Curve D -17 °F  
Min Metal Temp. at Required thickness (UCS 66.1) -21 °F

**MDMT Calculations in the Head Straight Flange:**

Govern. thk,  $t_g = 1.375$  ,  $t_r = 1.240$  ,  $c = 0.1181$  in. ,  $E^* = 1.00$   
Stress Ratio =  $t_r * (E^*) / (t_g - c) = 0.986$  , Temp. Reduction = 1 °F

Min Metal Temp. w/o impact per UCS-66, Curve D -17 °F  
Min Metal Temp. at Required thickness (UCS 66.1) -18 °F

Note: Post Weld Heat Treatment is required for this Element/Joint.

## Lampiran 15. Analisa PV Elite *External Pressure*

### **External Pressure Calculation Results :**

#### **ASME Code, Section VIII, Division 1, 2013**

#### **Elliptical Head From 20 to 30 Ext. Chart: CS-5 at 86 °F**

##### **BOTTOM HEAD**

Elastic Modulus from Chart: CS-5 at 86 °F : 0.302E+08 psi

Results for Maximum Allowable External Pressure (MAEP):

Tca	OD	D/t	Factor A	B
1.257	63.77	50.74	0.0027373	24773.69

EMAP = B / (K0\*D/t) = 24773.6875 / (0.9000 \* 50.7391 ) = 542.5068 psig

Results for Required Thickness (Tca):

Tca	OD	D/t	Factor A	B
0.160	63.77	398.19	0.0003488	5266.88

EMAP = B / (K0\*D/t) = 5266.8784 / (0.9000 \* 398.1908 ) = 14.6967 psig

*Check the requirements of UG-33(a)(1) using P = 1.67 \* External Design pressure for this head.*

Material UNS Number: K12437

Required Thickness due to Internal Pressure [tr]:

= (P\*D\*Kcor) / (2\*S\*E-0.2\*P) Appendix 1-4 (c)  
= (24.541\*61.2597\*0.995) / (2\*22900.00\*1.00-0.2\*24.541)  
= 0.0327 + 0.1181 = 0.1508 in.

Max. Allowable Working Pressure at given Thickness, corroded [MAWP]:

= ((2\*S\*E\*t) / (Kcor\*D+0.2\*t)) / 1.67 per Appendix 1-4 (c)  
= ((2\*22900.00\*1.00\*1.2569) / (0.995\*61.2597+0.2\*1.2569)) / 1.67  
= 563.261 psig

Maximum Allowable External Pressure [MAEP]:

= min( MAEP, MAWP )  
= min( 542.51 , 563.2607 )  
= 542.507 psig

*Thickness requirements per UG-33(a)(1) do not govern the required thickness of this head.*

#### **Cylindrical Shell From 30 to 40 Ext. Chart: CS-5 at 86 °F**

##### **SHELL**

Elastic Modulus from Chart: CS-5 at 86 °F : 0.302E+08 psi

Results for Maximum Allowable External Pressure (MAEP):

Tca	OD	SLEN	D/t	L/D	Factor A	B
1.257	63.77	211.02	50.74	3.3089	0.0010182	15374.11

$$EMAP = (4*B)/(3*(D/t)) = (4*15374.1074)/(3*50.7391) = 404.0040 \text{ psig}$$

Results for Required Thickness (Tca):

Tca	OD	SELEN	D/t	L/D	Factor A	B
0.329	63.77	211.02	193.93	3.3089	0.0001416	2137.51

$$EMAP = (4*B)/(3*(D/t)) = (4*2137.5088)/(3*193.9326) = 14.6959 \text{ psig}$$

Results for Maximum Stiffened Length (Slen):

Tca	OD	SELEN	D/t	L/D	Factor A	B
1.257	63.77	12861.87	50.74	50.0000	0.0004287	6473.52

$$EMAP = (4*B)/(3*(D/t)) = (4*6473.5190)/(3*50.7391) = 170.1125 \text{ psig}$$

### **Elliptical Head From 40 to 50 Ext. Chart: CS-5 at 86 °F**

#### TOP HEAD

Elastic Modulus from Chart: CS-5 at 86 °F : 0.302E+08 psi

Results for Maximum Allowable External Pressure (MAEP):

Tca	OD	D/t	Factor A	B
1.257	63.77	50.74	0.0027373	24773.69

$$EMAP = B/(K0*D/t) = 24773.6875/(0.9000 * 50.7391) = 542.5068 \text{ psig}$$

Results for Required Thickness (Tca):

Tca	OD	D/t	Factor A	B
0.160	63.77	398.19	0.0003488	5266.88

$$EMAP = B/(K0*D/t) = 5266.8784/(0.9000 * 398.1908) = 14.6967 \text{ psig}$$

*Check the requirements of UG-33(a)(1) using  $P = 1.67 * \text{External Design pressure for this head.}$*

Material UNS Number: K12437

Required Thickness due to Internal Pressure [tr]:

$$= (P*D*K_{cor})/(2*S*E-0.2*P) \text{ Appendix 1-4 (c)}$$

$$= (24.541*61.2597*0.995)/(2*22594.00*1.00-0.2*24.541)$$

$$= 0.0331 + 0.1181 = 0.1512 \text{ in.}$$

Max. Allowable Working Pressure at given Thickness, corroded [MAWP]:

$$= ((2*S*E*t)/(K_{cor}*D+0.2*t))/1.67 \text{ per Appendix 1-4 (c)}$$

$$= ((2*22594.00*1.00*1.2569)/(0.995*61.2597+0.2*1.2569))/1.67$$

$$= 555.734 \text{ psig}$$

Maximum Allowable External Pressure [MAEP]:

$$= \min( MAEP, MAWP )$$

$$= \min( 542.51, 555.7341 )$$

$$= 542.507 \text{ psig}$$

*Thickness requirements per UG-33(a)(1) do not govern the required thickness of this head.*

### **External Pressure Calculations**

Factor	From	To	Section Length ft.	Outside Diameter in.	Corroded Thickness in.	Factor A	Factor B psi
--------	------	----	-----------------------	-------------------------	---------------------------	----------	-----------------

Calc	10	20	4.92125	...	...	No Calc	No
24773.7	20	30	No Calc	63.7735	1.25689	0.0027373	
15374.1	30	40	17.5851	63.7735	1.25689	0.0010182	
24773.7	40	50	No Calc	63.7735	1.25689	0.0027373	

**External Pressure Calculations**

From	To	External Actual T. in.	External Required T. in.	External Des. Press. psig	External M.A.W.P. psig
10	20	...	No Calc	...	No Calc
20	30	1.37500	0.27827	14.6954	542.507
30	40	1.37500	0.44695	14.6954	404.004
40	50	1.37500	0.27827	14.6954	542.507
Minimum					404.004

**External Pressure Calculations**

From	To	Actual Len. Bet. Stiff. ft.	Allow. Len. Bet. Stiff. ft.	Ring Inertia Required in**4	Ring Inertia Available in**4
10	20	4.92125	No Calc	No Calc	No Calc
20	30	No Calc	No Calc	No Calc	No Calc
30	40	17.5851	1071.82	No Calc	No Calc
40	50	No Calc	No Calc	No Calc	No Calc

Elements Suitable for External Pressure.

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## Lampiran 16. Analisa PV Elite *Hidrostatic Pressure*

### **Hydrostatic Test Pressure Results:**

Pressure per UG99b	= 1.3 * M.A.W.P. * Sa/S	1176.320	psig
Pressure per UG99b[34]	= 1.3 * Design Pres * Sa/S	1169.005	psig
Pressure per UG99c	= 1.3 * M.A.P. - Head(Hyd)	1298.521	psig
Pressure per UG100	= 1.1 * M.A.W.P. * Sa/S	995.348	psig
Pressure per PED	= 1.43 * MAWP	1293.952	psig

### **UG-99(b), Test Pressure Calculation:**

$$\begin{aligned} &= \text{Test Factor} * \text{MAWP} * \text{Stress Ratio} \\ &= 1.3 * 904.862 * 1.000 \\ &= 1176.320 \text{ psig} \end{aligned}$$

### **Vertical Test performed per: UG-99b**

*Please note that Nozzle, Shell, Head, Flange, etc MAWPs are all considered when determining the hydrotest pressure for those test types that are based on the MAWP of the vessel.*

### **Stresses on Elements due to Test Pressure:**

From To	Stress	Allowable	Ratio	Pressure
BOTTOM HEAD	26406.8	29770.0	0.887	1184.67
SHELL	26985.0	29770.0	0.906	1184.05
TOP HEAD	26234.5	29770.0	0.881	1176.94

Elements Suitable for Internal Pressure.

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## Lampiran 17. Analisa PV Elite Wind Load

Wind Design Code		ASCE-7 95	
Basic Wind Speed	[V]	100.66	
mile/hr			
Surface Roughness Category		C: Open Terrain	
Importance Factor		1.0	
Type of Surface		Moderately Smooth	
Base Elevation		0.0000	ft.
Percent Wind for Hydrotest		33.0	
Using User defined Wind Press. Vs Elev.		N	
Height of Hill or Escarpment	H or Hh	0.0000	ft.
Distance Upwind of Crest	Lh	0.0000	ft.
Distance from Crest to the Vessel	x	0.0000	ft.
Type of Terrain ( Hill, Escarpment )		Flat	
Damping Factor (Beta) for Wind (Ope)		0.0100	
Damping Factor (Beta) for Wind (Empty)		0.0000	
Damping Factor (Beta) for Wind (Filled)		0.0000	

### Wind Analysis Results

Dynamic Gust-Effect Factor, Operating Case [Gf]:

$$= ( 1 + 2 * G * Zbar * \text{sqrt}( Q2 + R2 ) ) / ( 1 + 7 * Zbar )$$

$$= (1+2*3.500*0.228*\text{sqrt}(0.898+0.022)) / (1+7*0.228)$$

$$= 0.975$$

Natural Frequency of Vessel (Operating)	8.570 Hz
Natural Frequency of Vessel (Empty)	10.403 Hz
Natural Frequency of Vessel (Test)	9.258 Hz

Note: Per Section 1609 of IBC 2003/06/09 these results are also applicable for the determination of Wind Loads on structures (1609.1.1).

User Entered Importance Factor is	1.000
Force Coefficient	[Cf] 0.558
Structure Height to Diameter ratio	4.458
Height to top of Structure	23.045 ft.

*This is classified as a flexible structure. Dynamic analysis performed.*

### Sample Calculation for the First Element

The ASCE code performs all calculations in Imperial Units only. The wind pressure is therefore computed in these units.

Value of [Alpha] and [Zg]:

Exposure Category: C from Table C6-2  
Alpha = 9.500 : Zg = 900.000 ft.

Effective Height [z]:

= Centroid Height + Vessel Base Elevation  
= 2.461 + 0.000 = 2.461 ft.

Velocity Pressure coefficient evaluated at height z [Kz]:

$$\begin{aligned}
& \text{Because } z \text{ (2.461 ft.)} < 15 \text{ ft.} \\
& = 2.01 * ( 15 / Zg ) ^{(2 / Alpha)} \\
& = 2.01 * ( 15/900.000 )^{(2/9.500 )} \\
& = 0.849
\end{aligned}$$

Type of Hill: No Hill

As there is No Hill Present: [Kzt]:

$$K1 = 0, K2 = 0, K3 = 0$$

Topographical Factor [Kzt]:

$$\begin{aligned}
& = ( 1 + K1 * K2 * K3 )^2 \\
& = ( 1 + 0.000 * 0.000 * 0.000 )^2 \\
& = 1.0000
\end{aligned}$$

Velocity Pressure evaluated at height z, Imperial Units [qz]:

$$\begin{aligned}
& = 0.00256 * Kz * Kzt * Kd * I * Vr(\text{mph})^2 \\
& = 0.00256 * 0.849 * 1.000 * 1.000 * 1.000 * 100.662^2 \\
& = 22.0 \text{ psf}
\end{aligned}$$

Force on the first element [F]:

$$\begin{aligned}
& = qz * Gf * Cf * WindArea \\
& = 22.020 * 0.975 * 0.558 * 30.341 \\
& = 363.1 \text{ lb.}
\end{aligned}$$

Element	Hgt (z)	K1	K2	K3	Kz	Kzt
qz	ft.					
psf						
-----						
---						
SKIRT	2.5	0.000	0.000	0.000	0.849	1.000
22.020						
BOTTOM HEAD	5.0	0.000	0.000	0.000	0.849	1.000
22.020						
SHELL	13.3	0.000	0.000	0.000	0.849	1.000
22.020						
TOP HEAD	22.2	0.000	0.000	0.000	0.922	1.000
23.905						

### **Wind Vibration Calculations**

This evaluation is based on work by Kanti Mahajan and Ed Zorilla

#### **Nomenclature**

- Cf - Correction factor for natural frequency
- D - Average internal diameter of vessel ft.
- Df - Damping Factor < 0.75 Unstable, > 0.95 Stable
- Dr - Average internal diameter of top half of vessel ft.
- f - Natural frequency of vibration (Hertz)

f1 - Natural frequency of bare vessel based on a unit value of (D/L<sup>2</sup>) (10<sup>4</sup>)  
 L - Total height of structure ft.  
 Lc - Total length of conical section(s) of vessel ft.  
 tb - Uncorroded plate thickness at bottom of vessel in.  
 V30 - Design Wind Speed provided by user mile/hr  
 Vc - Critical wind velocity mile/hr  
 Vw - Maximum wind speed at top of structure mile/hr  
 W - Total corroded weight of structure lb.  
 Ws - Cor. vessel weight excl. weight of parts which do not effect stiff.  
 lb.  
 Z - Maximum amplitude of vibration at top of vessel in.  
 Dl - Logarithmic decrement ( taken as 0.03 for Welded Structures )  
 Vp - Vib. Chance, <= 0.200E+02 (High); 0.200E+02 < 0.250E+02 (Probable)  
 P30 - wind pressure 30 feet above the base

**Check other Conditions and Basic Assumptions:**

#1 - Total Cone Length / Total Length < 0.5  
 0.000/21.659 = 0.000  
 #2 - ( D / L<sup>2</sup> ) \* 10<sup>4</sup> < 8.0 (English Units)  
 - ( 5.27/21.66<sup>2</sup> ) \* 10<sup>4</sup> = 112.434 [Geometry Violation]

Compute the vibration possibility. If Vp > 0.250E+02 no chance. [Vp]:

= W / ( L \* Dr<sup>2</sup> )  
 = 35167 / ( 21.66 \* 5.105<sup>2</sup> )  
 = 0.62305E+02

Since Vp is > 0.250E+02 no further vibration analysis is required !

The Natural Frequency for the Vessel (Ope...) is 8.57048 Hz.

**Wind Load Calculation**

Element	From	To	Wind Height	Wind Diameter	Wind Area	Wind Pressure	Wind Load
			ft.	ft.	sq.in.	psf	lb.
10	20		2.46062	6.16534	4369.13	22.0201	363.138
20	30		5.00458	6.37735	153.056	22.0201	12.7212
30	40		13.2900	6.37735	15064.6	22.0201	1252.09
40	50		22.1578	6.37735	1152.66	23.9050	104.003

## Lampiran 18. Analisa PV Elite Seismic Load

### Earthquake Analysis Results

The UBC Zone Factor for the Vessel is ..... 0.1500  
 The Importance Factor as Specified by the User is . 1.000  
 The UBC Frequency and Soil Factor (C) is ..... 2.750  
 The UBC Force Factor as Specified by the User is .. 3.000  
 The UBC Total Weight (W) for the Vessel is ..... 37127.2 lb.  
 The UBC Total Shear (V) for the Vessel is ..... 5105.0 lb.  
 The UBC Top Shear (Ft) for the Vessel is ..... 0.0 lb.

The Natural Frequency for the Vessel (Ope...) is 8.57048 Hz.

### Earthquake Load Calculation

From	To	Earthquake Height ft.	Earthquake Weight lb.	Element Ope Load lb.	Element Emp Load lb.
10	20	2.46062	1913.05	50.5787	51.4594
20	30	5.00458	2033.79	109.363	111.267
30	40	13.2900	30855.6	4406.11	2823.83
40	50	21.5754	2324.82	538.946	548.330
Top Load		22.93		0	0

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## Lampiran 19. Analisa PV Elite MAWP Flange

### Nozzle Flange MAWP Results :

Nozzle Description Grade Group	----- Flange Rating Operating	Ambient	Temperature	Class
	psig	psig	°F	
-----				
N1 GR 1.1	1309.1	1480.0	302	600
N3 GR 3.8	1453.8	1500.0	302	600
N4 GR 1.1	1309.1	1480.0	302	600
N6 GR 1.1	1309.1	1480.0	302	600
N8 GR 3.8	1453.8	1500.0	302	600
K1 A GR 1.1	1309.1	1480.0	302	600
K1 B GR 1.1	1309.1	1480.0	302	600
K2 A GR 1.1	1309.1	1480.0	302	600
K2 B GR 1.1	1309.1	1480.0	302	600
K3 GR 3.8	1453.8	1500.0	302	600
K4 A GR 1.1	1309.1	1480.0	302	600
K4 B GR 1.1	1309.1	1480.0	302	600
K5 A GR 1.1	1309.1	1480.0	302	600
K5 B GR 1.1	1309.1	1480.0	302	600
M 1 GR 1.1	1309.1	1480.0	302	600
N2 GR 1.1	1309.1	1480.0	302	600
N5 GR 3.8	1453.8	1500.0	302	600
-----				
-----				
Minimum Rating	1309.100	1480.000	psig	(for Core Elements)

Note: ANSI Ratings are per ANSI/ASME B16.5 2009 Edition

## Lampiran 20. Analisa PV Elite Data *Nozzle*

### Nozzle Calculation Summary:

Description Areas or Stresses	MAWP psig	Ext	MAPNC psig	UG45 [tr]	Weld Path
-------------------------------------	--------------	-----	---------------	-----------	--------------

```

-----
---
N7          913.21      OK      ...      OK 0.307      OK
Passed
N1          913.21      OK      ...      OK 0.472      OK
Passed
N3          913.21      ...      ...      OK 0.296      OK
NoCalc[*]
N4          913.21      OK      ...      OK 0.363      OK
Passed
N6          913.21      OK      ...      OK 0.344      OK
Passed
N8          913.21      ...      ...      OK 0.296      OK
NoCalc[*]
K1 A       913.21      OK      ...      OK 0.344      OK
Passed
K1 B       913.21      OK      ...      OK 0.344      OK
Passed
K2 A       913.21      OK      ...      OK 0.344      OK
Passed
K2 B       913.21      OK      ...      OK 0.344      OK
Passed
K3          913.21      ...      ...      OK 0.296      OK
NoCalc[*]
K4 A       913.21      OK      ...      OK 0.344      OK
Passed
K4 B       913.21      OK      ...      OK 0.344      OK
Passed
K5 A       913.21      OK      ...      OK 0.344      OK
Passed
K5 B       913.21      OK      ...      OK 0.344      OK
Passed
M 1        913.21      OK      ...      OK 0.561      OK
Passed
N2          904.86      OK      ...      OK 0.437      OK
Passed
N5          904.86      OK      ...      OK 0.296      OK
Passed
N5          904.86      ...      ...      OK 0.296      OK
NoCalc[*]

```

---

[\*] - This was a small opening and the areas were not computed or

the MAWP of this connection could not be computed because the longitudinal bending stress was greater than the hoop stress.

Note: MAWPs (Internal Case) shown above are at the High Point.

Check the Spatial Relationship between the Nozzles

From Node Limit	Nozzle Description	Y Coordinate,	Layout Angle,	Dia.
20	N7	0.000	0.000	
6.962				
30	N1	138.220	180.000	
41.138				
30	N3	20.000	0.000	
5.114				
30	N4	86.000	0.000	
26.735				
30	N6	176.000	180.000	
24.836				
30	N8	98.000	180.000	
5.114				
30	K1 A	134.000	0.000	
24.836				
30	K1 B	89.000	90.000	
24.836				
30	K2 A	122.000	90.000	
24.836				
30	K2 B	62.000	180.000	
24.836				
30	K3	164.000	0.000	
5.114				
30	K4 A	50.000	0.000	
24.836				
30	K4 B	14.000	180.000	
24.836				
30	K5 A	56.000	90.000	
24.836				
30	K5 B	14.000	90.000	
24.836				
30	M 1	56.000	270.000	
45.138				
40	N2	0.000	0.000	
17.472				
40	N5	0.000	180.000	
7.930				

**The nozzle spacing is computed by the following:**

=  $\text{Sqrt}(l_l^2 + l_c^2)$  where

$l_l$  - Arc length along the inside vessel surface in the long. direction.

$l_c$  - Arc length along the inside vessel surface in the circ. direction

If any interferences/violations are found, they will be noted below.

No interference violations have been detected !

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