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AN OPTIMAL TUNING OF PSS USING AIS ALGORITHM FOR DAMPING OSCILLATION OF MULTI-MACHINE POWER SYSTEM

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ABSTRACT

This paper proposes an optimal tuning of Power System Stabilizer (PSS) using Artificial Immune System (AIS) algorithm for damping oscillation of multi-machine power system. PSS is the efficient devices to damp the power system oscillations which are caused by interruptions. This study presents a robust algorithm to determine the PSS parameters using AIS algorithm. The PSS parameters tuning is usually formulated as the objective function with constraints, including the damping ratio and damping factor. Optimization with maximum value of the damping factor and the damping ratio of power system modes are taken as the goals functions, when designing the PSS parameters. This optimization procedure could enhance the cloning process and lead to a better outcome. In this work, the two-area multi-machine power system of IEEE model, under a wide range of system configurations and operation conditions is investigated. The system has been used to illustrate the performance of the proposed algorithm. The performance of the AIS-based PSS is compared to the Delta w PSS and Delta Pa PSS. The results verify that, AIS-based PSS, Delta w PSS and Delta Pa PSS gives relatively good in reducing oscillation system variables of which transfer electrical power, changes in angular velocity generator, and the generator terminal voltage. All PSS can work well in order to stabilize the system under interruption. However, AISbased PSS have relatively better than Delta w PSS and Delta Pa PSS in terms of ability to reduce oscillation and speed of reaching a state of instability.

Keywords: Power System Stabilizer (PSS), Artificial Immune System (AIS) Algorithm, Optimal Tuning, Transient Stability, Damping Oscillation, Multi-Machine Power System.

1. INTRODUCTION

Power system stabilizer (PSS) is a device that used to mitigate system damping of low-frequency oscillations is an important control objective for optimization design in electrical power systems. The conventional tuning processes based on the linear approaches such as the eigenvalue analysis, for the linear parameters of the PSS tuning such as gain and time constants, have been used. Electrical power systems are often operated in situations of critical that may lead to instability cases and in worst-case blackouts [1]-[4]. In many of electric power systems around the world, the large interruptions have historically occurred [5]-[8]. This condition may lead to panic and state of emergency in the society, something to be avoided [9]-[10]. However, by focusing only on small signal

condition, the performance of dynamic damping immediately following a big disturbance is often degraded. The limits of PSS output can provide a solution to balance theses competing effects. In particular, these values of PSS limits attempt to prevent the machine terminal voltage from falling below the exciter reference level while the speed is also dropping. It means that it can improve the reduced transient recovery after a system disturbance [11]-[12]. The disturbances generally are in the form of short circuit caused both inside and outside of the system. The power system is often impaired the short circuit faults, either permanent or temporary. The short circuit fault can cause a deviation in voltage, current, frequency, and others. This deviation may affect the stability of the electric power system. The stability in the power

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avatam is defined as the	ability of the system to traditional DSS	The traditional DSS is able to

system is defined as the ability of the system to maintain the synchronization at the time of both interruption and after interruption occurs [13]-[15].

Increasing in intricacy of electric power systems has enhanced interests in developing the methodologies for PSS [16]-[18]. The effects of both transient and dynamic stability are among the main issues in the reliable and efficient operation of power systems. Low frequency oscillation modes have been observed when the multi-machine power systems are interconnected by weak tie-lines. The mode is also called the mode of electromechanical oscillation, and it usually happens in the frequency range of 0.1 to 2 Hz.

PSS is the most efficient device for damping both local mode and inter-area mode small signal low frequency oscillation by increasing the system damping. In large power system, the machines are equipped with PSS, which provides supplementary feedback and stabilizes the signal in the excitation system. The problem of PSS design is to tune the parameters of the stabilizer. The problem can cause the increase of damping of the system's electromechanical oscillation modes. The tune of PSS must be done without adverse effects on other oscillatory modes, such as those associated with the exciters or the shaft torsional oscillations. The PSS must also be so designed, that it has no adverse effects on a system's recovery from a severe fault. The concept and parameters of PSS have been considered in various studies. The PSS has been usually used for mitigating the influences low frequency oscillation.

PSS can enhance the dynamic stability of the power systems. PSS action is to expand the limits of the stability of bulk multi-machine power system by delivering synchronous machine rotor oscillation damping via the excitation generator [19]. Oscillation damping is provided by an electric torque applied to the rotor in line with variations of speed. On the other hand, the use of artificial intelligence (AI)-based algorithm has a lot of help in the field of bulk power systems [20]-[24]. The use of artificial intelligence (AI)-based algorithm is not only limited to the field of image processing [25]-[29]. In the last two decades, various methods have been applied to create design of PSS in order to improve the performance of the bulk power system. Most of the PSS model which is used in the power system was developed based on the classical linear control theory [30]-[31]. The linear control refers to a linear model of the power system configuration that is fixed value. Therefore, the PSS with fixed parameters are often called the

traditional PSS. The traditional PSS is able to function at its optimum for a particular operating condition in constant. The PSS is not effective for the operating conditions change drastically [32]-[39]. Therefore, in this study will be elaborated models of artificial immune system based technique for PSS tuning model in order to overcome the problem of transient stability of the multi-machine electrical power system. In this approach, it is conducted linearized model of the machines on interconnected electric power system. By this technique, it is expected to be obtained by a relatively simple method and suitable for overall electrical power system conditions that are various greatly.

2. POWER SYSTEM STABILIZER IN ELECTRICAL POWER SYSTEM

2.1. Power System Stabilizer Model

In bulk electrical power system, it is generally consists of a multi-machine system connected to an infinite bus. Growing in both generation and load of power system, the more vulnerable to interference, especially short-circuit interference. One effect of the interference is the oscillation of power that will cause the system out of the area of stability. It can also result in an even worse as a total blackout. The occurrence of short circuit faults in transmission line for the various types that is to disruption by 70% for one phase to ground fault, two-phase to ground fault by 10%, phase to phase fault by 15%, and symmetrical three-phase fault by 5%.

Stability of power system is characterized into both steady state and transient stabilities. Transient stability associated with the major interruption that occurs suddenly, like a short circuit faults, line disconnections, and removal or disconnection of the burden. On the other hand, the steady state stability associated with the ability of the power system to return to the conditions of its operating point after a small disturbance or rejection such as changes in power or load smoothly. The stability is also called dynamic stability. Small changes in load will result in a change in the angular velocity of the machine rotor, resulting change in terminal voltage of the machine. The angular velocity of the synchronous machine will swing around speed and voltage terminal converging around its rating voltage.

In the large multi-machine system, a system is said to be dynamically stable if there is after disturbance, the difference in the angle of the rotor head at a certain finite value. If there is a difference between the angles progressively enlarged, the

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system is called "unstable". Due to changes in the load on dynamic stability studies are relatively smalls, the multi-machine system model used in this study is a linearization of non-linear models. Small change in load on the system is a matter that could not be avoided and it is always the case. It is necessary to design a controller of power system that can maintain the system remains stable, commonly called Power System Stabilizer (PSS).

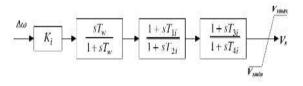


Figure 1. Typical structure of PSS

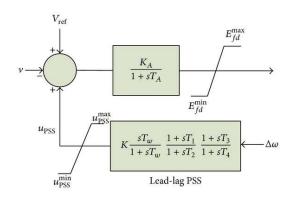


Figure 2. Typical Structure Of Ieee Type St1 Excitation System With Pss

The general function of a PSS is to generate appropriate torque on the machine rotor, in such a way that, the phase lag between the exciter input and the machine electrical torque is compensated. In many study, the extensively used speed based PSS design is considered where the stabilizing signal is assumed to be proportional to the speed perturbation. The typical structure of PSS is shown in Figure 1. It consists of a gain block with gain Ki, a signal washout block and two-stage phase compensation blocks.

Another type of PSS is shown in Figure 2. A PSS is placed with each synchronous generator. The PSS is used to provide an additional damping torque if system tempts to become unstable for oscillations. All PSSs are traditional PSS which consists of two-stage lead-lag compensation blocks with one gain and one washout block. The input of PSS is rotor speed deviation ($\Delta\omega$). Figure 2 shos the

IEEE type ST1 excitation system with PSS. In the figure, Tw is the washout time constant. Tw is set to 10 s for all PSSs. The parameters which are optimized consist of lead-lag time constants (T_1 , T_2 , T_3 , and T_4) and gain constant (K). Figure 3 shows block diagram of PSS in a control system.

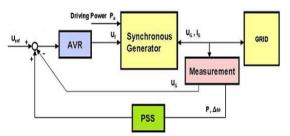


Figure 3. Block diagram of PSS in a control system

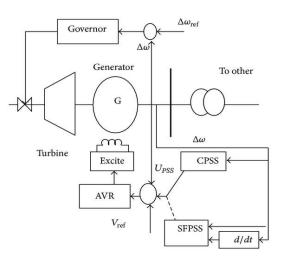


Figure 4. Position Of Pss In A Power Plant

The basic function of PSS is to expand the limits of stability by modulating the excitation machine to produce oscillation damping rotor synchronous machine. The oscillation of power is usually occurs within a frequency range of about 0.2 to 3.0 Hz. The oscillation can interfere with the rotor power frequency. The ability of the power system to transmit electrical power can be deteriorated. For damping these oscillations, PSS must be able to produce electric torque according to the changes of rotor speed. One example of the position of PSS in a power plant in addressing the stability of the power system is shown in Figure 4. <u>31st December 2016. Vol.94. No.2</u>

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2.2. Artificial Immune System Method

Artificial immune system (AIS) concept is used to explain the basic response of the immune system by being adaptive to antigen stimulation. The concept is described in Figure 5. This concept states that the only cells able to recognize antigens that will proliferate and the other cells are ignored. In the concept of AIS, the clonal selection operates on B cells and T cells in cell B, when the antibody binds to the antigen then activated and differentiated into plasma cells or memory cells. With respect to this process, B cell clones are produced and undergo somatic hyper-mutation. As the results, the diversity in the population of B cells to plasma cells produce antibodies antigen-specific works against antigens is obtained. As the consequence, the memory cells be left over with host antigens and promote secondary response quickly.

The important features of the artificial immune system type of clonal selection are:

- a. new cells are duplicates of those parents (called "clone") which is charged with the rapid mutation mechanism height (somatic hyper-mutation),
- b. the elimination of the new different lymphocyte causing it the self-reactive receptors,
- c. the proliferation and the differentiation takes place through connection adult cells with antigen, and
- d. the persistence of illegal clones, resistant to early elimination by self-antigen, is used as the basis of the auto-immune disease.

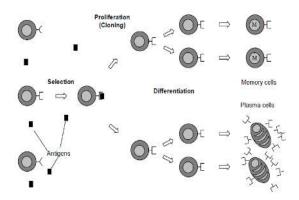


Fig. 5. The Principle Of Artificial Immune System

The analogy with selection of naturally fit the reality that is the strongest candidate into most cells recognizes antigens or into cells most triggered. To workings of this method, repertoire or population of receptors should be diverse enough to recognize any form of foreign cells. The immune system of a mammalian contains a heterogeneous repertoire of about 10^{12} lymphocytes in humans, and the rest of B cells (stimulated) can display about 10^5-10^7 identical like-antibody receptor. If the repertoire has been believed complete, it means that he can recognize the shape of any cell.

In [11], they have presented the algorithm of clonal selection, called "ClonalG" for optimization process. They proposed the important features of the concept of clonal selection and develop algorithms include the maintenance of a set of specific memory, selection and cloning antibodies are most stimulated, death antibody non-excitatory, maturation affinity. After that, the selection of reclones is balanced against affinity antigen, and the generation and maintenance of a set of antibodies.

The important steps of artificial immune system type of clonal selection are described below.

```
Input: Ab, gen, n, d, L, \beta;
Output: Ab, f
     for t = 1 to gen,
1.
1.1
    f := decode
                      (Ab);
                                       f
                              vector
     contains
                     all
                               affinity
     antibodies
                  that
                         bind
                                to
                                     the
     antigen
1.2
     Abn := select (Ab, f, n);
1.3
     \textbf{C} := clone (Abn, \beta, f);
1.4
     C* := hypermut (C, f);
1.5
     f := decode (C*);
1.6
     Abn := select (C*, f, n);
     Ab := insert (Ab, Abn);
1.7
1.8
     Abd := generate
                          (
                             d,
                                  L
                                     );
     randomly
                generate
                           antibody
     along L
1.9
     Ab := replace
                     (Ab,
                          Abd,
                               f);
     end:
2.
     f
                                  Decode
         :=
               decode
                         (Ab);
     functions
                  are
                         supposed
                                      to
                        evaluation
     encode
             Ab
                  and
                                     for
```

The affinity between antigen and antibody can be defined using different methods such as matching rules and a measure of distance. One common method used is the Euclidean distance. The method is suitable when using a real-valued vector representation. In order to explain the work of ClonalG using Euclidean distance, suppose $Ag = \{Ag_1, Ag_2, ..., Ag_N\}$, and $Ab = \{Ab_1, Ab_2, ..., Ab_N\}$ show the antigen and antibody sets respectively, N is the support of the order. After that, the degree of match between Ag and Ab. d can be calculated

values decode.

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based on the distance of Euclidean:

$$d = \sum_{i=1}^{N} (Ag_i - Ab_i)^2$$
(1)

And then, d compared with the threshold λ , and a matching error E is obtained using the equation:

$$\mathbf{E} = \mathbf{d} - \lambda \tag{2}$$

If E > 0, it is considered that the two vectors do not match, so that these antigens are not recognized by the antibody while if $E \le 0$, concluded that Ag Ab match, then the antigen recognized by the antibody. The common range for calculation of affinity is varying between 0 and 1.

For maturation of affinity, algorithm of ClonalG assumes that the n highest affinity antibody is sorted rise, and the number of clones that are raised for all n selected antibodies, which are given by:

$$Nc = \sum_{i=1}^{n} round\left(\frac{\beta \cdot N}{i}\right)$$
(3)

with N is the clones total number for each antigen, β are the cloned factor determining the scale factor for the clones number for antibodies elected and β common value is $\in (0,1]$, N is the antibodies total amount and round() is operators who rotate argument to the nearest integer. Every part of this amount corresponds to the clones size of each antibody chosen, for example, for N = 200 and β = 1, antibodies highest affinity (i = 1) will produce 200 clones, while the affinity of antibody the second highest yield of 100 clones, and thus further [11].

3. METHODOLOGY

In this study, an IEEE model multi-machine power system that are consists of two fully symmetrical areas is used. The areas are interconnected by the two 230 kV electrical power transmission lines of 220 km length. It was specifically designed to study low frequency electromechanical oscillations in large interconnected multi-machine electrical power systems. In the IEEE model, there are four synchronous which are interconnected in a system. Although the size of the system created in this study was relatively small, but already represents multimachine system in actual operation. The IEEE multi-machine power system circuit diagram model in this study is shown in Figure 6. The IEEE standard multi-machine power system consists of 4 generators and 13 buses by interference on the transmission line.

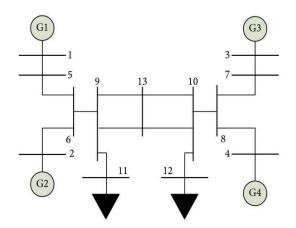


Figure 6. IEEE Model Multi-Machine Power System Of 4 Generators And 13 Buses By Interconnection On The Transmission Line

Figure 7 shows an IEEE model of multimachine power system under study. Each area of the system is equipped with the two identical synchronous generators round rotor types rated of 20 kV and 900 MVA. The synchronous generators have assumed identical parameters, except for inertias which are H = 6.7s for area 1 and H = 6.25sfor area 2. The thermal plants having assumed the identical speed regulators are further assumed at all locations. It is in addition to fast static exciters with a 400 gain.

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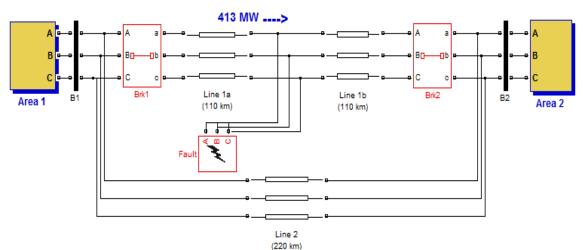


Figure 7. A Two Area Multi-Machine Power System Under Study

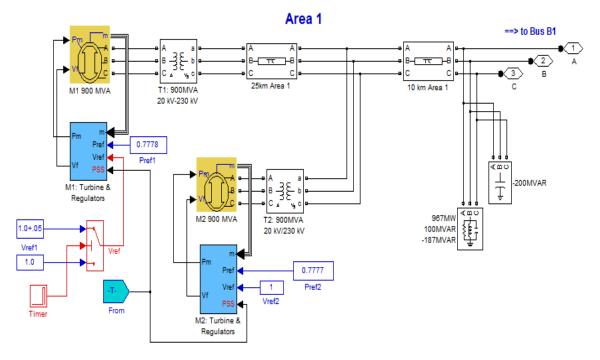


Figure 8. Configuration Of Area 1 Of Multi-Machine Power System

Journal of Theoretical and Applied Information Technology 31st December 2016. Vol.94. No.2 © 2005 - 2016 JATIT & LLS. All rights reserved. ISSN: 1992-8645 E-ISSN: 1817-3195 www.jatit.org Area 2 38 в 7-8 8-1 75 7-8 C . 's 0 С С ==> to Bus B2 25km Area 2 10 km Area 2 T3: 900MVA M3 900 MVA •1 20 kV-230 kV А 2 в Pref 0.798889 3 Pref3 Vref 1 С Vref3 PSS M3: Turbine & -38 Regulators Ľв ≪ @ 0 v₅ 0 Ţ 350MVAR M4 900 MVA T4: 900MVA 20 kV/230 kV ņ 1767MW ŧ Pref 0.7778 100MVAR -187MVAR From Vret 1 Pref4 PSS Vref4 M4: Turbine & Regulators

Figure 9. Configuration Of Area 2 Of Multi-Machine Power System

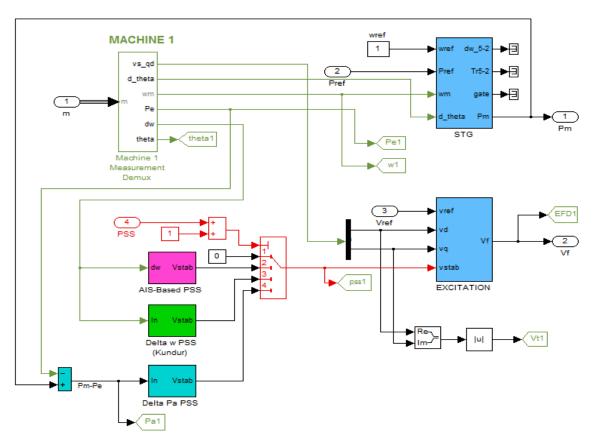


Figure 10. PSS Model With AIS-Based Method In Machine 1 Of Area 1 Under Study

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The IEEE model of multi-machine power system in this study is shown in Figure 7. It can be seen in Figure 7 that the multi-machine power system has two areas which is interconnected by the transmission lines. Figure 8 shows the configuration of multi-machine power system components of area 1 while Figure 9 shows configuration of components of area 2 of IEEE model multi-machine power system under study.

In the IEEE model of multi-machine power system under study, the load of the system is represented as constant impedances and split between the two areas. The area 1 is exporting 413MW to area 2. The multi-machine system is somewhat stressed, even in steady-state, because the surge impedance loading of a single line is 140 MW. The reference power flow with generator M2 considered the slack machine is such that all generators are producing the active power about 700 MW. In this work, the power losses of transmission and generation may vary depending on the detail level in power transmission line and generator parameter representation.

4. RESULTS AND DISCUSSION

4.1 Multi-machine Power System Analysis for Small Signal

In this work, an IEEE model of multi-machine power system analysis for small signal is examined. In order to comprehend the behavior of the network, the open-loop responses to a magnitude pulse of 5% is applied for 12 cycles at the generator M1 voltage reference. By using the simulink toolbox, simulation is started by opening the timer controlling the generator M1 voltage reference and changing the factor of multiplication of the transition time vector from 100 to 1. After that, the power transmission line fault should be deactivated by changing from 1 to 100 the factor of multiplication of the transition time vector in the fault device and transmission line breakers. And then, the signals responses are visualized by opening the scopes of "Machine" and "System" on the main diagram as shown in Figure 7.

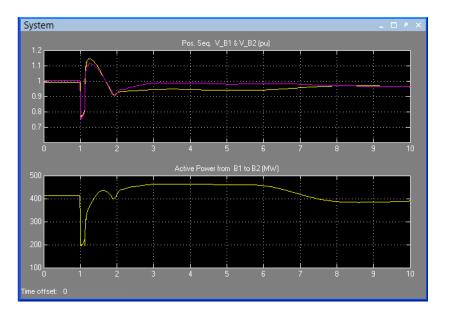


Figure 11. The Signals Of The System Scope Under Simulation In Simulink

Figure 10 shows the PSS model with AIS-based method in machine 1 of area 1 of multi-machine power system under study. The PSS model with AIS-based is compared with another PSS model, i.e. Delta w PSS and Delta Pa PSS. As input data for both PSS model with AIS-based method and Delta w PSS is the same, namely a change in

angular velocity (dw) while input data for Delta Pa PSS is the difference between the mechanical power (Pm) and electric power (Pe) of generator under study. Then, the signals of the system scope under simulation in simulink software have been shown in Figure 11 while the signals of the four machine scopes have been shown in Figure 12. As

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can be seen in Figure 11 and Figure 12,	all signals	configuration of all component	of area 2 of multi-

can be seen in Figure 11 and Figure 12, all signals show undamped oscillations leading to unstable. A modal analysis of acceleration powers of all generators shows the three dominant modes, i.e.:

- a. Mode of inter-area (fn = 0.66Hz , z = -0.028) involving the whole area 1 against area 2. This mode is clearly observable in the tie-line power displayed in scope of "System".
- b. Area 1 using local mode (fn = 1.14Hz, z = 0.09) involving this area's machines against each other.
- c. Area 2 using local mode (fn = 1.17Hz, z = 0.09) involving generator M₃ against generator M₄ (in this case, the smaller the inertia then the greater the frequency of local natural).

From Figure 8 and Figure 9, if the circuit breakers both Brk_1 and Brk_2 are setting in the position of open circuit, then one of the two tielines of the circuit is removed. Figure 8 shows the configuration of all component of area 1 of multimachine power system while Figure 9 shows the machine power system. Each area has the two synchronous machines with the capacity of 900 MVA. Each of the machine is equipped with the 20/230 kV power transformer with the capacity of 900 MVA. It is possible to reach the point of steady-state stable equilibrium with the same patterns of load and power generation. This phenomenon is named a post-contingency network. The post-contingency network can be initialized using the Machine and Load-Flow Initialization toolbox in simulink software feature. After that, analysis in modal type for the network's responses to the same 5% of magnitude pulse could be done. By the analysis, it can be understood that it was applied for 12 cycles at the voltage reference of generator M₁ reveals that. Therefore, at this time the two local modes has been remain basically unchanged in both natural frequency and damping factor, i.e. fn=1.10Hz, z=0.09 in area 1, and fn=1.18Hz, z=0.09 in area 2. And then, the interarea mode will shift to a lower frequency with unstable condition, i.e. fn = 0.45Hz and z = -0.017.

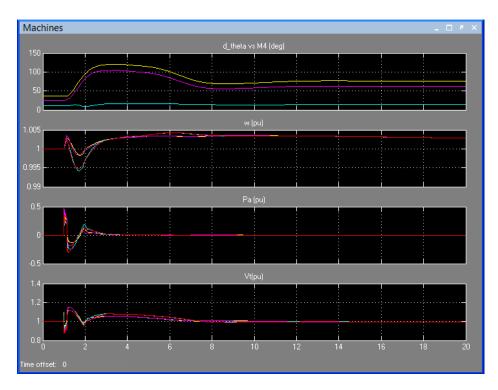


Figure 12. The Signals Of The Generator Scope Under Simulation

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4.2 Tuning of AIS-based PSS for Multi-machine Power System

In this study, the AIS-based PSS setting is created in matlab m-file, and then the file is connected to the PSS model in simulink environmental. In order to examine the AIS-based which is proposed in this work, it has been simulated another PSS scheme, i.e. delta w PSS and delta Pa PSS, as shown in Figure 10. The results of bode plot of all PSS scheme in this work is shown in Figure 13. For the Delta w PSS, the setting data are from Kundur [18]. The Delta w PSS settings have two changes i.e. a gain increase from 25 to 30 and a 15-ms transducer time constant. The frequency responses of all the three PSS in this simulation can be seen on Bode Plot of all PSS in Figure 13. Based on the the figure, it can be seen that the AIS-based PSS, which is proposed in this study, is effectively flat around 25-40 degrees in the frequency range of interest. As a comparison, Delta w PSS has an overall poor phase shape, especially around the frequency of 1-2 Hz. By this fact, there makes it unable to cope with faster local or intermachine modes in multi-unit power system. Thus, for Delta Pa PSS, it has a good performance in combination of strong gain and phase advance above frequency of 0.3 Hz. However, the Delta Pa PSS type is unpractical at low frequency. From bode plot diagram, it shows a 180 degrees phase advance, which actually has a destabilizing effect despite the rather small low-frequency gain. For the third PSS scheme, Delta w PSS, the low-frequency shaping is satisfactory in overall, but its DC rejection is not efficient enough. This frequency condition is providing five times less attenuation than the proposed AIS-based PSS.

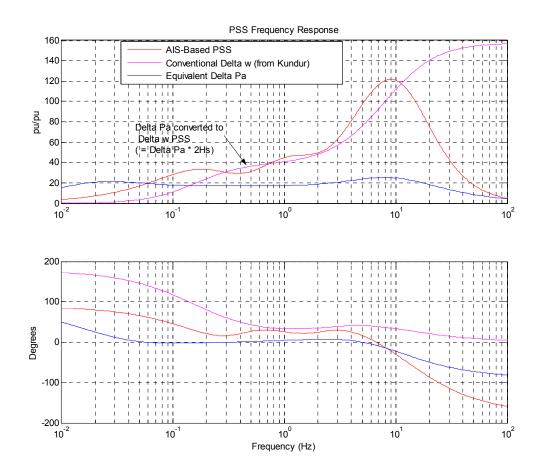


Figure 13. Bode Plot Of All PSS Under Simulation

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4.3 Small-Signal Performance Assessment of AIS-based PSS

In this part, the small-signal performance assessment of AIS-based PSS is explained. In order to examine the small-signal with closed-loop system responses of the PSS, the transition time vector of circuit breakers and all fault devices on the main diagram should be disabled by multiplying it by 100. After that, the timer block is used to control the reference of voltage of generator M1. the timer block is activated in the same way by removing any multiplication by 100, i.e. by changing 100 to 1. For comparison to another two PSS model in this simulation, it can be done b selecting the PSS model by setting PSSmodel = 1, 2, or 3. Once the PSS model is selected, then the simulation can be started and the output variables could be recorded. Most of the variables, for example terminal voltage and generator speed, are stored in matrices W and Vt. It can be seen inside both blocks of Machines and System on the main diagram for other variables. This procedure can be repeated for the all the three PSSs for performance comparison. In order to examine the comparisons, it can be done by double clicking on icon Show results: Step on vref of generator M1. The simulation results of this part are show in 12-cycle pulse of 5% of voltage reference magnitude of generator M1, as presented in Figure 14. The figure have four plots, i.e. the top one shows the power transfer from area 1 to area 2, the second one is the generator M1 speed, the third one is acceleration power of generator M1 and the bottom one is the terminal voltage of generator M1.

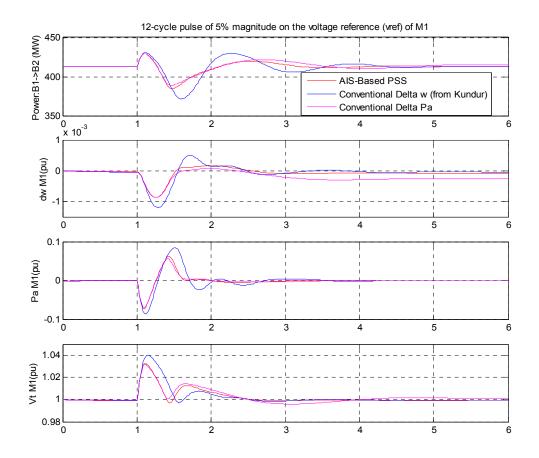


Figure 14. 12-Cycle Pulse Of 5% Of Voltage Reference Magnitude Of Generator M1

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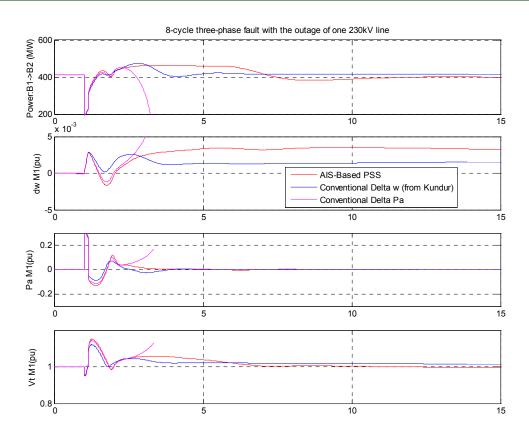


Figure 15. 8-Cycle Symmetrical Three Phase Fault With The Outage Of 30 Kv Transmission Line

Figure 14 shows four variables of 12-cycle pulse of 5% of voltage reference magnitude of generator M_1 , i.e. power transfer from area 1 to area 2, angular velocity change, power of generator M_1 , and terminal voltage of generator M₁, respectively. In Figure 14, it can be seen that all PSSs have a nice in stabilizing the naturally unstable system. However, if compared with another to PSS, the AIS-based PSS is superior. The AIS-based PSS provides significantly more damping to all modes, especially with respect to the Delta w PSS. The Delta w PSS is poor gain shaping above frequency of 0.5 Hz while the proposed AIS-based PSS have good performance. For overall, the damping performance of the interarea-mode with two ties of multi-machine power system for all PSS is: AISbased PSS: fn = 0.4Hz and z = 0.35; Delta w PSS: fn = 0.64Hz and z = 0.25; Delta Pa PSS: fn = 0.35Hz and z = 0.30. For damping performance of the interarea-mode with two ties multi-machine power system for all PSS is: AIS-based PSS: fn =

0.42Hz and z = 0.37; Delta w PSS: fn = 0.43Hz and z = 0.35; Delta Pa PSS: fn = 0.23Hz and z = 0.14.

4.4 Large-Signal Performance Assessment of AIS-based PSS

In this part, the large-signal performance assessment of all PSS model is explained. In order to assess the proposed AIS-based PSS, small-signal performance is not enough. Therefore, the largesignal performance is needed. Figure 15 shows 8cycle three phase fault with the outage of 230 kV power transmission line. The robust performance during large perturbations is one of the criteria of PSS characteristic assessment. Another criterion of an equal importance is good robustness with respect to changing operating conditions. The system response to a symmetrical three-phase fault cleared in 8 cycles by opening both the breaker Brk₁ and Brk₂ can be simulated by using the same procedure as above. The multi-machine power system can reach a stable operating point in steady-state in

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condition of without one tie-line. By the simulation, not every PSS is able to ensure a smooth transition into this new highly stressed operating point.

Figure 15 shows four variables 8-cycle symmetrical three phase fault with the outage of 30 kV transmission line, i.e. power transfer from area 1 to area 2, angular velocity change, power of generator M₁, and terminal voltage of generator M₁, respectively. From figure 15, it can be seen that for implementation of Delta Pa PSS, the system lost its synchronism while both AIS-based PSS and Delta w PSS succeed in maintaining the power system stability. The latter are both AIS-based PSS and Delta w PSS highly effective in damping the oscillation of the power transfer. From the simulation, it can be shown that the closed-loop oscillation frequency of the AIS-based is lower. For Delta w PSS, it is too slow on recovering the terminal voltage. In addition, the acceleration of power is more damped with the proposed AISbased PSS model than any other PSS, as can be seen in Figure 15. It is an advantage of the proposed AIS-base PSS compared to the two others PSS.

5. CONCLUSION

In our research, AIS-based PSS has been successful in controlling the multi-machine power system under study. Multi-machine power system consists of four generators. Application testing on the generator M1 to symmetrical three-phase short circuit fault, it is resulted that the proposed AISbased PSS have good design in this study. All PSS in this study, i.e. AIS-based PSS, Delta w PSS and Delta Pa PSS, have given relatively good results in reducing oscillation system variables of which transfer electrical power, changes in angular velocity generator, and generator terminal voltage. However, the performance of the proposed AISbased PSS have relatively better than Delta w PSS and Delta Pa PSS in terms of ability to damp oscillation and speed of reaching a stability state. Based on this study, it can be seen that the proposed AIS-based PSS rapidly deliver good results compared with Delta w PSS and Delta Pa PSS primarily on the state of the multi-machine power system.

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